

(REVISION OF ANSI B1.12-1972)

REAFFIRMED 1998

FOR CURRENT COMMITTEE PERSONNEL PLEASE SEE ASME MANUAL AS-11

Class 5 Interference-Fit Thread



The American Society of Mechanical Engineers Intentionally left blank

Ashthorhoc.com.cide.to

Class 5 Interference-Fit C.COM. Click to view the **Thread**

ASME/ANSI B1.12-1987

(REVISION OF ANSI B1.12-1972)



The American Society of Mechanical Engineers

Date of Issuance: November 15, 1987

This Standard will be revised when the Society approves the issuance of a new edition. There will be no addenda or written interpretations of the requirements of this Standard issued to this edition.

This code or standard was developed under procedures accredited as meeting the criteria for American National Standards. The Consensus Committee that approved the code or standard was balanced to assure that individuals from competent and concerned interests have had an opportunity to participate. The proposed code or standard was made available for public review and comment which provides an opportunity for additional public input from industry, academia, regulatory agencies, and the public-at-large.

ASME does not 'approve,'' "rate," or "endorse" any item, construction, proprietary device, or activity.

ASME does not take any position with respect to the validity of any patent rights asserted in connection with any items mentioned in this document, and does not undertake to insure anyone utilizing a standard against liability for infringement of any applicable Letters Patent, nor assume any such liability. Users of a code or standard are expressly advised that determination of the validity of any such patent rights, and the risk of infringement of such rights, is entirely their own responsibility.

Participation by federal agency representative(s) or person(s) affiliated with industry is not to be interpreted as government or industry endorsement of this code or standard.

ASME accepts responsibility for only those interpretations issued in accordance with governing ASME procedures and policies which preclude the issuance of interpretations by individual volunteers.

No part of this document may be reproduced in any form, in an electronic retrieval system or otherwise, without the prior written permission of the publisher.

Copyright © 1987 by
THE AMERICAN SOCIETY OF MECHANICAL ENGINEERS
All Rights Reserved
Printed in U.S.A.

FOREWORD

(This Foreword is not part of ASME/ANSI B1.12-1987.)

Interference-fit threads are threads in which the externally threaded member is larger than the internally threaded member when both members are in the free state and which, when assembled, become the same size and develop a holding torque through elastic compression, plastic movement of material, or both. By custom, these threads are designated as Class 5.

Tentative Class 5 fit threads were first published by the National Screw Thread Commission (1928), and alternate Class 5 appeared in the 1944 Handbook H28. These standards were helpful in stabilizing design; however, in spite of restrictive tolerances, loosening or breakage of externally threaded members has been all too frequent. Also, minimum and maximum torque values were established, the validity of which has been generally accepted.

The tentative and alternate standards, which were based on National Bureau of Standards and industry research, testing, and field study, represent the first attempt to establish an American standard for interference-fit threads. These specifications are published in Appendix A. In 1947, ASA Sectional Committee B1 on Screw Threads established Subcommittee 10 under the chairmanship of Harry Marchant to study the problems of interference fits. A subgroup of the subcommittee, chaired by W. S. Brown, conducted a comprehensive survey of design, production, and driving practices in the automotive, implement, railroad, and fastener industries and found that all were experiencing difficulty. Typical problems were:

- (a) the variety of materials and heat treatments used for externally threaded members;
- (b) variations resulting from rolling, outring, or grinding external threads;
- (c) the huge variety of chemical analyses and physical and mechanical properties encountered in the forged, cast, die cast, and rolled materials into which the externally threaded members are driven;
 - (d) the widely varying effects of chemical coatings, platings, and lubricants; and
 - (e) the inability to closely control sizes of tapped holes in various materials.

It was impossible to establish a standard at that time, but it was agreed that interference-fit threads could not be eliminated in design of equipment and that a workable standard was essential.

In 1951, Subcommittee 10, later renumbered 12, established a research subgroup which conducted extensive tests under a variety of conditions. The work of this research subgroup and a report of subsequent research and field experience is described in the article "New Class 5 Interference Fit Thread" by W. G. Waltermire, which appeared in the September 6, 1956 issue of *Machine Design*.

This Trial American Standard was predicated on the following conclusions, which were drawn from the research and field experience for developing holding torque through plastic movement of materials.

- (a) Materials of the external and internal interference-fit threads compress elastically and flow during assembly and when assembled.
- (b) During driving, plastic flow of materials occurs, resulting in either an increase of the external thread major diameter or a decrease in the internal thread minor diameter, or both.
- (c) Relieving the external thread major diameter and the internal thread minor diameter to make allowance for plastic flow eliminates the main causes of seizing, galling, and abnormally high and erratic driving torques.

- (d) Relieving the major diameter of external threads and minor diameter of internal threads requires an increase in the pitch diameter interference in order to obtain driving torques within the range established. (In driving studs, it was found that the minimum driving torque should be about 50% greater than the torque required to break loose a properly tightened nut.)
- (e) Lubricating only the internal thread results in more uniform torques than lubricating only the external thread and is almost as beneficial as lubricating both external and internal threads. Some applications do not permit lubrication.
- (f) For threads having truncated profile, torque increases directly as the pitch diameter interference for low interferences, but torque soon becomes practically constant and increases little, if at all, with increases of interference. Obviously, for uniformity of driving torques, it is desirable to work with greater interferences, resulting in plastic flow of materials.
- (g) Comparatively large pitch diameter interferences can be tolerated, provided the external thread major diameter and internal thread minor diameter are adequately relieved and proper lubrication is used during assembly.
- (h) Driving torque increases with turns of engagement, but levels off after the assembly is well advanced. (For thin wall applications, it may be desirable to use longer engagement and smaller pitch diameter interference to obtain desired driving torque.)
- (i) Studs should be driven to a predetermined depth. Bottoming or shouldering must be avoided. Bottoming, which is engagement of the threads of the stud with the imperfect threads at the bottom of a shallow drilled and tapped hole, causes the stud to stop suddenly during power driving, thus inviting failure in torsional shear. Slipping clutches may permit transmission of excess torque. Bottoming can also damage parts having only a weak diaphragm at the bottom of the hole, through either mechanical or hydrostatic compression. Shouldering, which is the practice of driving the stud until the thread runout engages with the top threads of the hole, may create excessive radial compressive stresses and upward bulging of the material at the top of the hole. The torque, or stud holding power, produced by these radial compressive stresses is considerably relieved when the tensile load is applied to the stud, and may be inadequate to prevent backout in service.

The Trial American Standard was issued in November 1959. On October 23, 1961, the subcommittee reviewed the standard and recommended republication, without technical change, as an American Standard. It was felt that the lack of adverse comment after 2 years existence as a Trial Standard, and the reception of favorable comments of usage, warranted this step. On May 16, 1963, the standard was formally designated an American Standard. Several errors were discovered and B1.12 was rewritten. It was approved on September 5, 1972.

The most recent research on interference-fit thread was conducted by the Portsmouth Naval Shipyard on both hardened steel and nickel-copper-aluminum (K Monel) studs assembled in alloy steel (HY-80), corrosion resistant steel, nickel-copper (Monel), copper-nickel, and nickel-chromium (Inconel) internal threads, and on nonferrous studs in nonferrous internal threads. They modified the B1.12 Class 5 specifications for plastic flow interference-fit threads when nickel-copper-aluminum external threads are assembled in many materials. They also provided more cavity space. A summary of their findings for developing holding torque through plastic flow and elastic compression of material follows.

- (a) Pitch diameter interferences specified in ANSI B1.12 were found to be too large, resulting in excessive failures.
 - (b) Lead, flank angles, taper, straightness, and roundness are important.
 - (c) Optimum surface roughness is 63 μ in. Ra.
- (d) Difference between functional size and pitch diameter of both the internal and external threads are measured and may not exceed 50% of the pitch diameter tolerances. (One foreign standard specifies 25%.)
- (e) Critical applications require selective fits, using measured pitch diameters on the external and internal threads, to obtain a specified interference when the external and internal threads are assembled.

- (f) Assembly torque cannot be continuous. Several waiting periods are required to let friction heat dissipate.
- (g) Studs are indexed to monitor their movement. Assembly is considered a failure if there is stud rotation when seating the prevailing torque nut or breaking it away.

These Portsmouth Naval Shipyard thread specifications are published in Appendix B for elastic interference where permanent distortion is not desired and Appendix C for plastic flow interference with extra allowance at both the crest and root for K Monel.

ASIME NO RIMO C. COM. Click to view the full POF of ASIME BI. 12 1981

Intentionally left blank

Ashthorhoc.com.cide.to

PDF of ASME B1.12,1981 **ASME STANDARDS COMMITTEE B1** Standardization and Unification of Screw Threads

(The following is the roster of the Committee at the time of approval of this Standard.)

OFFICERS

D. J. Emanuelli, Chairman H. W. Ellison, Vice Chairman C. E. Lynch, Secretary

COMMITTEE PERSONNEL

AEROSPACE INDUSTRIES ASSOCIATION OF AMERICA, INC.

- F. H. Cantrell, McDonnell Douglas Corp., St. Louis, Missouri
- H. Borrman, Alternate, Sperry Defense Electronics, Great Neck New York

AMERICAN MEASURING TOOL MANUFACTURERS ASSOCIATION

- P. F. Bitters, Greenfield, Massachusetts
- C. W. Jatho, Alternate, American Measuring Tool Manufacturers Association, Birmingham, Michigan

AMERICAN PIPE FITTINGS ASSOCIATION

W. C. Farrell, Jr., Stockham Valves and Fittings, Inc., Birmingham, Alabama

DEFENSE INDUSTRIAL SUPPLY CENTER

- E. Schwartz, Defense Industrial Supply Center, Philadelphia, Pennsylvania
- F. S. Ciccarone, Alternate, Defense Industrial Supply Center, Philadelphia, Pennsylvania

ENGINE MANUFACTURERS ASSOCIATION

G. A. Russ, Cummins Engine Co., Columbus, Indiana

INDUSTRIAL FASTENERS INSTITUTE

- R. M. Harris, Bethlehem Steel Corp., Lebanon, Pennsylvania
- K. E. McCullough, SPS Technologies, Inc., Newton, Pennsylvania
- J. C. McMurray, Russell, Burdsall & Ward Corp., Cleveland, Ohio
- J. A. Trilling, Holo-Krome Co., West Hartford, Connecticut C. J. Wilson, Industrial Fasteners Institute, Cleveland, Ohio

MANUFACTURERS STANDARDIZATION SOCIETY OF THE VALVE AND FITTINGS INDUSTRY

W. C. Farrell, Jr., Stockham Valves and Fittings, Inc., Birmingham, Alabama

METAL CUTTING TOOL INSTITUTE (TAP & DIE DIVISION)

A. D. Shepherd, Jr., Union/Butterfield Division, Litton Industrial Products, Derby Line, Vermont

NATIONAL ELECTRICAL MANUFACTURERS ASSOCIATION

- J. B. Levy, General Electric Co., Schenectady, New York
- F. F. Weingruber, Westinghouse Electric Corp., Pittsburgh, Pennsylvania
- T. A. Farkas, Alternate, National Electrical Manufacturers Association, Washington, D.C.

NATIONAL FASTENER DISTRIBUTORS ASSOCIATION

J. F. Sullivan, Accurate Fasteners, Inc., Boston, Massachusetts

NATIONAL MACHINE TOOL BUILDERS ASSOCIATION

- R. J. Sabatos, The Cleveland Twist Drill Co., Cleveland, Ohio
- B. V. Shook, Teledyne Landis Machine Co., Waynesboro, Pennsylvania

SOCIETY OF AUTOMOTIVE ENGINEERS

H. W. Ellison, General Motors Corp., Warren, Michigan

SOCIETY OF MANUFACTURING ENGINEERS

- D. M. Davidson, Lone Star Grinding Co., Southfield, Michigan
- L. E. Gibson, Alternate, Lone Star Grinding Co., Houston, Texas

TUBULAR RIVET AND MACHINE INSTITUTE

R. M. Byrne, Trade Association Management Inc., Tarrytown, New York

U.S. DEPARTMENT OF THE ARMY

- R. S. LaNier, Watervliet Arsenal, Watervliet, New York
- M. E. Taylor, U.S. Army Command, Dover, New Jersey
- F. L. Jones, Alternate, U.S. Army Missile Command, Redstone Arsenal, Alabama

U.S. DEPARTMENT OF THE NAVY

C. T. Gustafson, Metrology Laboratory, Portsmouth Naval Shipyard, Portsmouth, New Hampshire

INDIVIDUAL MEMBERS

- J. E. Boehnlein, PMC Industries, Wickliffe, Ohio
- A. R. Breed, Lakewood, Ohio
- R. Browning, Southern Gage Co., Erin, Tennessee
- R. S. Chamerda, The Johnson Gage Co., Bloomfield, Connecticut
- P. H. Drake, Hudson, Massachusetts
- D. J. Emanuelli, TRW-Greenfield Tap and Die, Greenfield, Massachusetts
- C. G. Erickson, Sterling Die Operation, West Hartford, Connecticut
- J. O. Heize, Regal Beloit Corp., South Beloit Illinois
- S. P. Johnson, The Johnson Gage Co., Bloomfield, Connecticut
- S. I. Kanter, The Hanson-Whitney Go. Hartford, Connecticut
- R. W. Lamport, The Van Keuren Co., Watertown, Massachusetts
- M. M. Schuster, Hi-Shear Corp. Corrance, California
- R. E. Seppey, Allied/Bendix Aerospace Corp., South Bend, Indiana
- A. G. Strang, Boyds, Maryland
- R. L. Tennis, Caterpilla Tractor Co., Peoria, Illinois
- A. F. Thibodeau, Swanson Tool Manufacturing, Inc., West Hartford, Connecticut

SUBCOMMITTEE B1.12 - CLASS 5 INTERFERENCE-FIT THREADS

- A. G. Strang, Chairman, Boyds, Maryland
- ESchwartz, Secretary, Defense Industrial Supply Center, Philadelphia, Pennsylvania
- R. F. Braun, Eastman Kodak Co., Rochester, New York
- P. E. Burke, American Motors Corp., Detroit, Michigan
- R. S. Chamerda, The Johnson Gage Co., Bloomfield, Connecticut
- A. E. Ellis, Bedford, Massachusetts
- H. W. Ellison, General Motors Corp., Warren, Michigan
- D. J. Emanuelli, TRW-Greenfield Tap and Die, Greenfield, Massachusetts
- D. M. Foote, Sanford, Florida
- C. T. Gustafson, Portsmouth Naval Shipyard, Portsmouth, New Hampshire
- G. A. Jannison, Puget Sound Naval Shipyard, Bremerton, Washington
- G. A. Russ, Cummins Engine Co., Columbus, Indiana
- R. H. Searr, Ingersoll-Rand Canada, Sherbrooke, Quebec, Canada
- R. E. Seppey, Allied/Bendix Aerospace Corp., South Bend, Indiana
- R. R. Stevens, Texas Instruments, Colorado Springs, Colorado
- C. J. Wilson, Industrial Fasteners Institute, Cleveland, Ohio

CONTENTS

| Forew | ord | | رقان |
|--------|----------|--|------|
| Standa | rds Com | mittee Roster | vii |
| | | | |
| 1 | Genera | il | 1 |
| | 1.1 | Scope | 1 |
| | 1.2 | Field of Application | 1 |
| | 1.3 | Reference Documents | 1 |
| | 1.4 | Acceptability | 1 |
| | 1.5 | Reference Temperature | 2 |
| | 1.6 | Units of Measure | 2 |
| | 1.7 | Federal Government Use | 2 |
| 2 | To smale | ology | 2 |
| 2 | | | 2 |
| | 2.1 | General | |
| | 2.2 | Additional Definitions Designations Class 5 External Thread Class 5 Internal Thread | 2 |
| 3 | Thread | Designations | 2 |
| | 3.1 | Class 5 External Thread | 2 |
| | 3.2 | Class 5 Internal Thread | 3 |
| | 3.2 | olds 5 Internal Throad | |
| 4 | Screw | Thread Profile | 3 |
| | 4.1 | Basic Profile | 3 |
| | 4.2 | Design Profiles | 3 |
| | 4.3 | Maximum and Minimum Interference | 3 |
| | 4.4 | Formulas | 3 |
| _ | ^ | | _ |
| 5 | | Thread Series | 3 |
| | 5.1 | Standard Series | 3 |
| | 5.2 | Fine Pitch Series | 3 |
| 6 | Screw | Thread Class | 8 |
| | | | |
| 7 | Screw | Thread Allowances and Tolerances | 8 |
| | 7.1 | Allowances | 8 |
| | 7.2 | Tolerances | 8 |
| 8 | Standa | ard Series Threads and Formulas for Limits of Size | 8 |
| o | 8.1 | Basic Dimensions for Standard Series Threads | 8 |
| _ | | | |
| 9 | | Characteristics | 10 |
| | 9.1 | Limits of Size | 12 |
| | 9.2 | Pitch Diameter Limits | 12 |
| | 9.3 | Major Diameter Limits | 12 |
| | 9.4 | Minor Diameter Limits | 12 |
| | 9.5 | Other Screw Thread Characteristics | 12 |
| | 9.6 | Length of Engagement | 12 |

| 10 | Notes on Product Design and Application | 12 |
|--------|--|----------|
| | 10.1 Conditions of Usage | 12 |
| | 10.2 External Threaded Products | 12 |
| | 10.3 Internal Threaded Products | 18 |
| | 10.4 Lead and Angle Variations | 18 |
| | 10.5 Cavity Space for Interference Material | 18 |
| | 10.6 Thread Axis Position | 18 |
| | 10.7 Surface Roughness | 18 |
| | 10.8 Lubrication | 20 |
| | 10.9 Driving Speed | 20 |
| | 10.10 Relation of Driving Torque to Length of Engagement | 20 |
| | 10.11 Breakloose Torques | 20 |
| 11 | Product Screw Thread Acceptability | 20 |
| | 11.1 Gaging Systems | 20 |
| | 11.2 Product Thread Characteristics Conformance Requirements Over Length of | |
| | Engagement for Gaging Systems 22 and 23 | 21 |
| 12 | Torque Pes Basic Thread Profile | 21 |
| '- | Torque | 21 |
| | | |
| Figur | res V | |
| 1 | | 4 |
| 2 | Design Profile for External NC-5 HF/CSF/ONF Thread | 5 |
| 3 | Design Profile for Internal NC-5 IF/INF Thread | 6 |
| 4 | Maximum and Minimum Interference | 7 |
| 5 | Illustration of LE , T_s , Tolerance of T_s , and T_h Required for Assembled | |
| | Threads | 13 |
| | es click to | |
| T. 61. | | |
| Table | Standard NC-5 Thread Series | 8 |
| 2 | Allowances for Coarse Thread Series | 9 |
| 3 | Tolerances for Pitch Diameter, Major Diameter, and Minor Diameter for | , |
| 3 | Coarse Thread Series | 9 |
| 4 | Basic Dimensions for Coarse Thread Series. | 10 |
| 5 | Thread Constants | 11 |
| 6 | External Thread Dimensions for Class 5 Standard | 14 |
| 7 | Internal Thread Dimensions for Class 5 Standard | 15 |
| 8 | Interferences, Engagement Lengths, and Torques for Class 5 Standard | 16 |
| 9 | Maximum Allowable Variations in Lead and Maximum Equivalent Change | |
| | in Functional Diameter | 19 |
| 10 | Maximum Allowable Variation in 30 deg. Basic Half-Angle of External | |
| No. | and Internal Screw Threads | 20 |
| . 11 | Working Gages | 22 |
| 12 | Setting Gages | 25 |
| | | |
| _ | | |
| | endices | |
| Α | Obsolete Tentative Standard and Alternate Standard for Class 5 | ~~ |
| | Interference-Fit Thread | 27 |
| | A1 Introduction | 27 |
| | A2 Tentative Standard | 27 27 |
| | A3 Alternate Standard | 41 |

| В | Specifications for Elastic interference in the care in | 43 |
|------------|--|----|
| | Di introduction | 43 |
| | DE Initua Designation il | 43 |
| | B3 External and Internal Threads Compared to NC-5 | 43 |
| | B4 Application Practice for New and Reworked External and Internal Threads | 44 |
| | B5 Gaging | 45 |
| С | Class 5 Modified Specifications for Plastic Flow Interference-Fit | |
| | Thread With Addition of K Monel External Thread | 49 |
| | C1 Introduction | 49 |
| | C2 Additions to Thread Designation Letters | 49 |
| | C3 External and Internal Threads Compared to ASME/ANSI B1.12 Class 5 | |
| | N V | 49 |
| | 1 iii Çudib | 50 |
| | | 50 |
| | C5 Tipphoution Tiutile Tot Tie Walle | 50 |
| | | - |
| D | Comparison of Interference Metal for the Thread Assemblies | |
| | Tabulated in the Appendices With the American National Standard | |
| | Oldas o Hillard Modelliplice | 55 |
| | D1 Explanation for Table D1 | 55 |
| | D1 Explanation for Table D1 | 55 |
| | | |
| | | |
| Figur | es | |
| A 1 | Illustration of Tolerances, Allowances, and Crest Clearances for Tentative | |
| | und intomate class o in isi immunit in | 28 |
| A2 | Illustration of Loosest Condition for Tentative Class 5 Wrench Fit for | |
| | Imoudou brade, 12 mm, 15 mm and, 47 mm | 29 |
| A3 | Illustration of Tightest Condition for Tentative Class 5 Wrench Fit for | |
| | Initiation States, 12 mill, 12 million and 12 milli | 29 |
| A4 | Illustration of Loosest Condition for Alternate Class 5 Fit for Threaded | |
| | Study, 12 mi, 15 millions, 500millions | 34 |
| A5 | Illustration of Tightest Condition for Alternate Class 5 Fit for Threaded | |
| | Studs, ½ in., 13 Threads. Set in Hard Materials | 34 |
| | | |
| | | |
| Table | s M | |
| A1 | Tentative Class 5 Wrench Fit for Threaded Studs, Allowances and | |
| | Tolerances for Studs and Tapped Holes, Coarse Threaded Studs Set in | |
| | Tidia indicates in the control of th | 30 |
| A2 | Tentative Class 5 Wrench Fit for Threaded Studs, Allowances and | |
| | Tolerances for Studs and Tapped Holes, Fine Threaded Studs Set in | |
| | I I I I I I I I I I I I I I I I I I I | 31 |
| A3 | Limiting Dimensions for Tentative Class 5 Wrench Fit for American | |
| | National Coarse Thread Series, Steel Studs Set in Hard Materials (Cast | |
| | Hon, bolinstool, bronze, ctor) | 32 |
| A4 | Limiting Dimensions for Tentative Class 5 Wrench Fit for American | |
| | National Fine Thread Series, Steel Studs Set in Hard Materials (Cast | |
| | from, boundades, bronzes, every treatment and the second s | 33 |
| A5 | Alternate Class 5 Fit for Threaded Studs, Allowances and Tolerances for | |
| | Otaus and Tapped Hotes, Course Timenate Transfer | 35 |
| A6 | Alternate Class 5 Fit for Threaded Studs, Allowances and Tolerances for | _ |
| | Studs and Tapped Holes, Fine Threaded Studs Set in Hard Materials | 35 |

| Α7 | Thread Series, Steel Studs Set in Hard Materials (Cast Iron, Semisteel, Bronze, etc.) | . 36 |
|------|--|------|
| A8 | Limiting Dimensions for Alternate Class 5 Fit, American National Fine Thread Series, Steel Studs Set in Hard Materials (Cast Iron, Semisteel, | . 30 |
| | Bronze, etc.) | 37 |
| A9 | Limiting Dimensions of Setting Plug and Thread Working Gages and Plain Diameter Gages for Alternate Class 5 Fit Threaded Studs, American National Coarse Thread Series | 38 |
| A10 | Limiting Dimensions of Thread Working Gages and Plain Diameter Gages for Alternate Class 5 Fit Tapped Holes, American National Coarse Thread Series | 39 |
| A11 | Limiting Dimensions of Setting Plug and Thread Working Gages and Plain Diameter Gages for Alternate Class 5 Fit Threaded Studs, American National Fine Thread Series | 40 |
| A12 | Limiting Dimensions of Thread Working Gages and Plain Diameter Gages for Alternate Class 5 Fit Tapped Holes, American National Fine Thread Series. | 41 |
| . В1 | External Thread Dimensions for NC-5 HFM. | 46 |
| B2 | Internal Thread Dimensions for NC-5 IFM | 46 |
| B3 | Engagement Length, Hole Depth, Interference, and Torque for NC-5 HFM and NC-5 IFM | 47 |
| B4 | Setting Gages for NC-5 HFM and NC-5 IFM. | 48 |
| C1 | External Thread Dimensions for Class 5 Modified for Nickel-Copper- | 50 |
| C2 | External Thread Dimensions for Class Modified for Greater Cavity Space | 51 |
| C3 | Space | 52 |
| C4 | Interference on Pitch Diameter for Class 5 Modified | 53 |
| D1 | Thread Assemblies Compared by Percentage of Interference Metal per | 5.0 |
| | Thread Assemblies Compared by Percentage of Interference Metal per Turn | 56 |
| ASM | | |

CLASS 5 INTERFERENCE-FIT THREAD

1 GENERAL

1.1 Scope

This Standard provides dimensional tables for external and internal plastic flow interference-fit (Class 5) threads of modified National thread form in the coarse thread series (NC) in sizes 0.250 in. through 1.500 in. This is not the ANSI B1.1 UN thread form. It is intended that designs conforming with this Standard will provide adequate torque conditions which fall within the limits shown in Table 8. The minimum torques are intended to be sufficient to insure that externally threaded members will not loosen in service; the maximum torques establish a ceiling below which seizing, galling, or torsional failure of the externally threaded components is reduced. This Standard provides for the maximum allowable interference.

Appendices A, B, C, and D contain useful information that is supplementary to this Standard, such as reprints of the obsolete tentative and alternate Class standards, U.S. Navy ship specifications for elastic interference-fit coarse thread series from 0.250 in. through 2.000 in., U.S. Navy ship specifications for Class 5 Modified which includes nickel-copper-aluminum alloy external threads, and an interference metal comparison of standard to nonstandard interference-fit threads.

1.2 Field of Application

Interference-fit threads provide a high degree of resistance against turning of studs when prevailing torque nuts are used and against loosening of studs caused by load cycling and vibration. These threads are not intended for use where regular removal for component maintenance is required.

1.3 Reference Documents

1.3.1 American National Standards. The latest issues of the following standards form a part of this Standard to the extent specified herein.

ANSI B1.1

Unified Inch Screw Threads (UN and UNR Thread Form)

ANSI/ASME B1.2

Gages and Gaging for Unified Inch Screw Threads

ANSI/ASME B1.3M

Screw Thread Gaging Systems for Dimensional Acceptability—Inch and Metric Screw Threads (UN, UNR, UNJ, M, and MJ)

ANSI/ASME B1.7M

Nomenclature, Definitions, and Letter Symbols for Screw Threads

ANSI B94.9

Taps Cut and Ground Threads

1.3.2 Other References

Metal Cutting Tool Institute. Taps, Ground Thread, Standards and Dimensions. Cleveland, 1983.

Society of Manufacturing Engineers.² Tool and Manufacturing Engineers Handbook—Volume 1, Machining.

American Society for Metals. Metals Handbook—Volume 3, Machining.

Metal Cutting Tool Institute. Metal Cutting Tool Hand-

Waltermire, W. G. "New Class 5 Interference Fit Thread." *Machine Design* (September 6, 1956): 83–96.

1.4 Acceptability

Acceptability of product screw threads, based on the gaging method specified, shall be in accordance with ANSI/ASME B1.3M. Gages and gaging are in accordance with ANSI/ASME B1.2 but with gaging dimensions as specified in Tables 11 and 12. See paras. 11.1.1, 11.1.2, and 11.1.3.

¹1230 Keith Building, Cleveland, Ohio 44115-2180.

²One SME Drive, P.O. Box 930, Dearborn, Michigan 48128.

³Metals Park, Ohio 44073.

1.5 Reference Temperature

The reference temperature is 68°F (20°C) for dimensions listed.

1.6 Units of Measure

All dimensions and values are expressed in inches unless otherwise noted.

1.7 Federal Government Use

When this Standard is approved by the Department of Defense and federal agencies and is incorporated into FED-STD-H28/23, Screw Thread Standards for Federal Services, Section 23, the use of this Standard by the federal government will be subject to all requirements and limitations of FED-STD-H28/23.

Appendices B and C are standard for U.S. Navy ship use.

2 TERMINOLOGY

2.1 General

For definitions, terms, and symbols relating to screw threads, see ANSI/ASME B1.7M.

2.2 Additional Definitions

breakaway or breakloose torque — torque required to start disassembly of the prevailing torque nut, or torque required to start disassembly of stud from internal threaded part

Class 5 fit — an interference-fit thread class used for interchangeable threaded members which are to be assembled by a turning force

elastic interference — an interference-fit assembly where the interference material zone is stressed within elastic limits. Upon disassembly, the thread profile usually has not been distorted.

ferrous material — iron and steel

galling — fracturing and tearing of the alloying mating surfaces and displacement of fractured metal particles during assembly or disassembly, caused by lack of lubrication, frictional heat, poor geometry of threads, and surface welding

lubricant — a liquid, powder, or mixture of both which permits assembly with a minimum of galling

lute — an ingredient of a lubricant such as graphite, rubber, white lead, molybdenum disulfide, or zinc dust maximum driving torque — the maximum assembly torque derived from past experimentation which prevents torsional external thread failure

minimum driving torque— the minimum assembly torque for an acceptable assembly based on a torque which is 50% larger than the breakaway torque of the prevailing torque nut

plastic flow interference — an interference-fit assembly where part of the interference zone materials are permanently displaced beyond elastic limits. The external thread material tends to flow mostly toward its major diameter and the internal thread material tends to flow toward the minor diameter.

resin sealer — an anaerobic plastic cement used to glue and lock the assembly together where service temperatures do not exceed 200°F and interference tolerances are not met, where fire safety is not a factor, or where UN Class 3A and 3B threads are used

sealer — a lubricant which is insoluble in the medium being used

torque — the force required for rotation of the screw multiplied by the perpendicular distance from the axis of the screw (expressed in pound-inches or pound-feet)

3 THREAD DESIGNATIONS

The following examples of external and internal thread designations provide the means for distinguishing the present standard Class 5 thread from the obsolete tentative and alternate American National Class 5 threads which are given in Appendix A.

NOTE: ANSI/ASME B1.3M permits gaging systems to be designated in general notes, purchasing specifications, company standards, etc., in which case the individual designation of the thread designation may be omitted.

3.1 Class 5 External Thread

3.1.1 For Driving in Hard Ferrous Material With Brinell Hardness Over 160 HB

EXAMPLE: 0.500-13 NC-5 HF ()

where

0.500 = nominal size

13 = threads per inch

 $N \,=\, American \; National \; thread \; form \;$

C = coarse thread series

5 = Class 5 American National tolerance

HF = hard ferrous material, external thread

() = System 21, 22, or 23

3.1.2 For Driving in Copper Alloy and Soft Ferrous Material With Brinell Hardness of 160 HB or Less

EXAMPLE: 0.500-13 NC-5 CSF () where

0.500 = nominal size

13 = threads per inch

N = American National thread form

C = coarse thread series

5 = Class 5 American National tolerance

CSF = copper alloy or soft ferrous material, external thread

() = System 21, 22, or 23

3.1.3 For Driving in Nonferrous Material Other Than Copper Alloys, Any Hardness

EXAMPLE: 0.500-13 NC-5 ONF ()

0.500 = nominal size

13 = threads per inch

N = American National thread form

C = coarse thread series

5 = Class 5 American National tolerance

NF = other nonferrous material except copper alloy, external thread

() = System 21, 22, or 23

3.2 Class 5 Internal Thread

3.2.1 Entire Ferrous Material Hardness Range

EXAMPLE: 0.500-13 NC-5 IF ()

where

0.500 = nominal size

13 = threads per inch

N = American National thread form

C = coarse thread series

5 = Class 5 American National tolerance

I = internal thread

F = entire ferrous material hardness range

() = System 21, 22, or 23

3.2.2 Entire Nonferrous Material Hardness

Range

EXAMPLE: 0.500-13 NC-5 INF ()

where

0.500 = nominal size

13 = threads per inch

N = American National thread form

C = coarse thread series

5 = Class 5 American National tolerance

I = internal thread

NF = entire nonferrous material hardness range

() = System 21, 22, or 23

4 SCREW THREAD PROFILE

The basic profile and design profiles are defined herein and are the bases for the thread dimensions in this Standard.

4.1 Basic Profile

The basic profile for National Class 5 interference threads is identical to the UN, UNR, and ISO 68 metric screw thread profile and is shown in Fig. 1.

4.2 Design Profiles

The design profiles define the maximum material conditions for external and internal threads and are derived from the basic profile.

4.2.1 Design Profile of External Threads. The design profile of external NC-5 screw threads is shown in Fig. 2. The crest is further truncated by adding an allowance to provide adequate cavity space for the displaced interference metal. Note that the NC-5 HF threads have the greater crest truncation.

The design profile of external NC-5 screw threads has flat crests and roots.

4.2.2 Design Profile of Internal Threads. The design profile of internal NC-5 screw threads is shown in Fig. 3.

4.3 Maximum and Minimum Interference

The maximum and minimum interference conditions for an assembly of 0.500-13 NC-5 HF hard ferrous external thread in a 0.500-13 NC-5 IF ferrous internal thread are illustrated in Fig. 4.

4.4 Formulas

Procedures to be applied to the basic profile for the limits of size of the National coarse series are given in Sections 7 and 8.

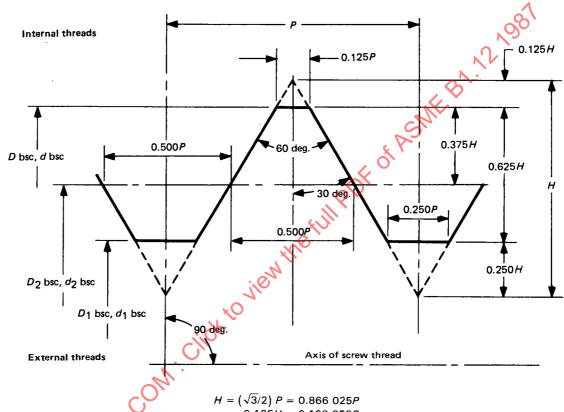
5 SCREW THREAD SERIES

5.1 Standard Series

The standard series consists of a coarse pitch series ranging from 0.250 in. through 1.500 in. (See Table 1.)

5.2 Fine Pitch Series

The fine pitch series is not part of this Standard and is not recommended.



 $0.125H = 0.108\ 253P$

 $0.250H = 0.216\ 506P$

0.375H = 0.324760P0.625H = 0.541266P

FIG. 1 BASIC THREAD PROFILE

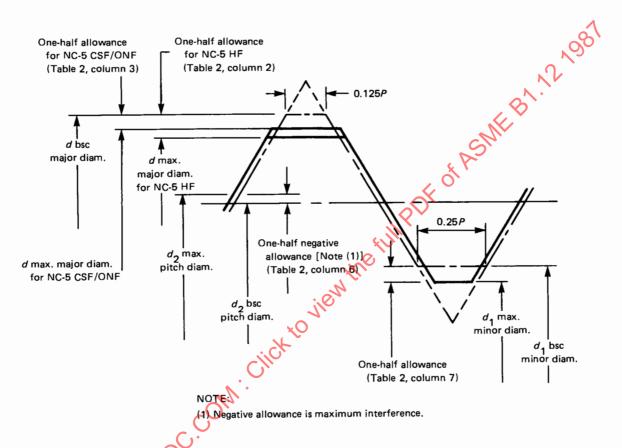
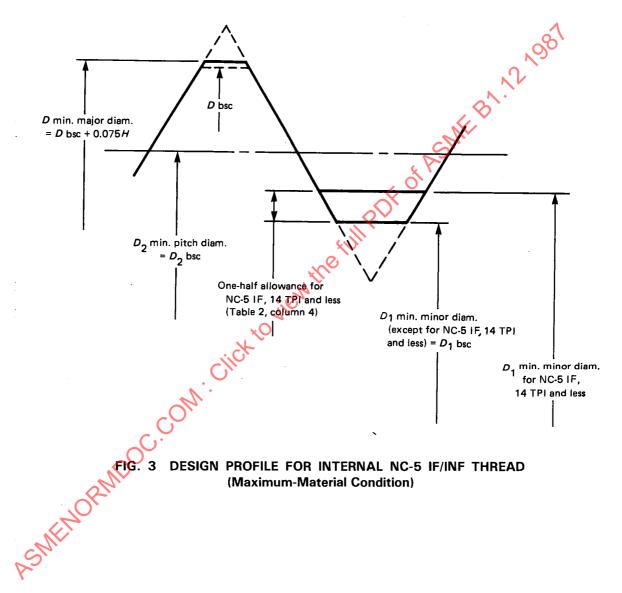
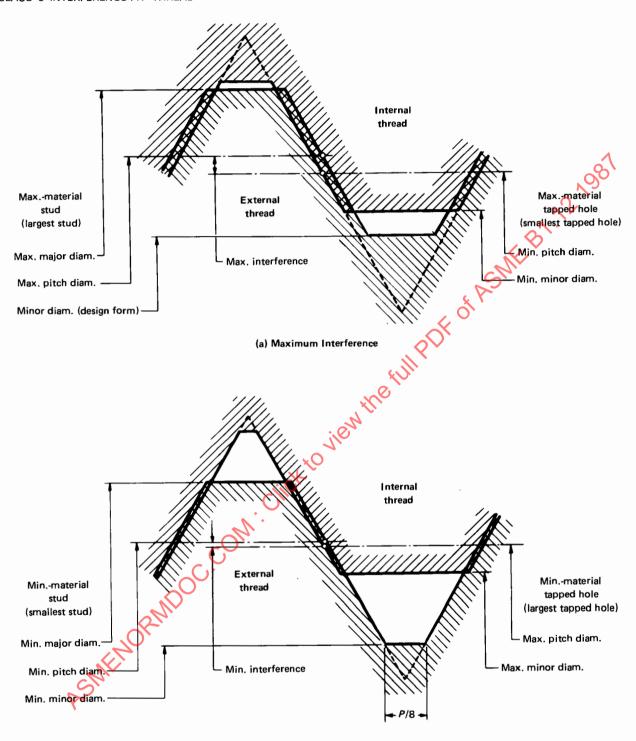


FIG. 2 DESIGN PROFILE FOR EXTERNAL NC-5 HF/CSF/ONF THREAD
(Maximum-Material Condition)





(b) Minimum Interference

GENERAL NOTES:

(a) 1/2-13 size is illustrated.

(b) Plastic flow of interference metal into cavities at major and minor diameter is not illustrated.

FIG. 4 MAXIMUM AND MINIMUM INTERFERENCE

| 1/4-20 | or | 0.2500-20 | 3/4-10 | or | 0.7500-10 |
|----------------------------|----|-----------|---------------------------|----|-----------|
| 5/16-18 | or | 0.3125-18 | ⁷ /8- 9 | or | 0.8750- 9 |
| 3/8-1 6 | or | 0.3750-16 | 1 - 8 | or | 1.0000- 8 |
| ⁷ /16-14 | or | 0.4375-14 | 1½- 7 | or | 1.1250- 7 |
| 1/2-13 | or | 0.5000-13 | 11/4- 7 | or | 1.2500- 7 |
| ⁹ /16-12 | or | 0.5625-12 | 13/8- 6 | or | 1.3750- 6 |
| ⁵ ∕8− 11 | or | 0.6250-11 | 11/2- 6 | or | 1.5000- 6 |
| | | | | | |

TABLE 1 STANDARD NC-5 THREAD SERIES

6 SCREW THREAD CLASS

The Class 5 interference fit was originally published as tentative by the National Screw Thread Commission in 1928. Over the years, some of the tolerances, diameters, and negative allowances (maximum interferences) have been modified in accordance with industry research.

7 SCREW THREAD ALLOWANCES AND TOLERANCES

7.1 Allowances

7.1.1 Pitch Diameter Allowance. A negative allowance (maximum pitch diameter interference) at maximum material is specified for the Class 5 external thread. Its purpose is to provide interference metal-to-metal contact to provide very high resistance to disassembly of the mated thread. (See Table 2.) There is no formula to generate the allowance.

7.1.2 Crest and Root Allowances. Crest and root allowances, tabulated in Table 2, such as differences between nominal size and maximum major diameter for external thread, between nominal size and minimum major diameter for internal thread (see General Notes to Table 2), between basic minor diameter and minimum minor diameter for internal thread, and between maximum minor diameter and basic minor diameter for external thread, provide cavity space at the major and minor diameters of Class 5 threads. These allowances are intended to reduce installation torques. These cavities accept displaced material from thread flank interference. (See para. 10.5.)

7.2 Tolerances

7.2.1 Pitch Diameter Tolerance. The pitch diameter tolerance for both internal and external threads is the same as for National Class 3. (See Table 3.) There

is no formula to generate the National Class 3 pitch diameter tolerance.

7.2.2 Major Diameter Tolerance

7.2.2.1 External Threads. The major diameter tolerance for all external threads is twice the National Class 3 pitch diameter tolerance. (See Table 3.)

7.2.2.2 Internal Threads. The major diameter limits for all internal threads are the limits published by the Metal Cutting Tool Institute for the major diameter for ground thread taps, and are given in this Standard as a reference for the internal thread major diameter. These limits are used in the design of the tools that produce the internal thread major diameter. Acceptance of the internal thread major diameter is by the acceptance of the thread by a maximum material GO thread gage. (See Table 3 for tap major diameter tolerance.)

7.2.3 Minor Diameter Tolerance. The minor diameter tolerances for internal threads are tabulated in Table 3. For NC-5 IF threads with 20 through 16 TPI and 6 through 4 TPI, and for all NC-5 INF threads, the minor diameter tolerances are those for National Class 3 internal minor diameter rounded to three decimal places. Minor diameter tolerances for the remaining threads for NC-5 IF are one-sixth of ${}^{3}\!\!/_{4}H$ or 0.125H rounded to three decimal places.

8 STANDARD SERIES THREADS AND FORMULAS FOR LIMITS OF SIZE

8.1 Basic Dimensions for Standard Series Threads

The standard series for National Class 5 screw threads is listed in Table 1. Basic dimensions are given for coarse thread series in Table 4. Thread form data is given in Table 5. The limits of size are established by applying tolerances and allowances to the basic dimensions as indicated. These limits are the basis for measuring and gaging of the thread.

TABLE 2 ALLOWANCES FOR COARSE THREAD SERIES

| TPI | Difference Between Nominal Size and Max. Major Diam. of NC-5 HF [Note (1)] | Difference Between Nominal Size and Max. Major Diam. of NC-5 CSF or NC-5 ONF [Note (1)] | Difference Between Basic Minor Diam. and Min. Minor Diam. of NC-5 IF [Note (1)] | Difference Between Basic Minor Diam. and Min. Minor Diam. of NC-5 INF | Maximum PD Interference or Negative Allowance, External Thread [Note (2)] | Difference Between Max. Minor Diam. and Basic Minor Diam., External Thread |
|-----|---|---|---|--|---|---|
| 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 20 | 0.0030 | 0.0030 | 0.000 | 0.000 | 0.0055 | 0.0072 |
| 18 | 0.0045 | 0.0035 | 0.000 | 0.000 | 0.0065 | 0.0080 |
| 16 | 0.0060 | 0.0040 | 0.000 | 0.000 | 0.0070 | 0.0090 |
| 14 | 0.0070 | 0.0045 | 0.014 | 0.000 | 0.0080 | 0.0103 |
| 13 | 0.0080 | 0.0050 | 0.014 | 0.000 | 0.0084 | 0.0111 |
| 12 | 0.0085 | 0.0050 | 0.016 | 0.000 | 0.0092 | 0.0120 |
| 11 | 0.0110 | 0.0055 | 0.017 | 0.000 | 0.0098 | 0.0131 |
| 10 | 0.0140 | 0.0060 | 0.019 | 0.000 | 0.0105 | 0.0144 |
| 9 | 0.0150 | 0.0065 | 0.022 | 0.000 | 0.0116 | 0.0160 |
| 8 | 0.0165 | 0.0065 | 0.025 | 0.000 | 0.0128 | 0.0180 |
| 7 | 0.0180 | 0.0070 | 0.030 | 0.000 | 0.0143 | 0.0206 |
| 6 | 0.0190 | 0.0070 | 0.034 | 0.000 | 0.0172 | 0.0241 |

GENERAL NOTE:

The difference between basic major diameter and internal thread minimum major diameter is 0.075H and is tabulated in Table 3, column 6.

NOTES:

- (1) The allowance values in columns 2, 3, and 4 were obtained from industrial research data.
- (2) Negative allowance is the difference between the basic pitch diameter and the pitch diameter value at maximum material.

TABLE 3 TOLERANCES FOR PITCH DIAMETER, MAJOR DIAMETER, AND MINOR DIAMETER FOR COARSE THREAD SERIES

| ТРІ | Pitch Diameter Tolerance for External and Internal Thread [Note (1)] | Major Diameter Tolerance for External Thread [Note (2)] | Minor Diameter Tolerance for Internal Thread NC-5 IF | Minor Diameter Tolerance for Internal Thread NC-5 INF [Note (3)] | Tolerance 0.075 <i>H</i> or 0.065 <i>P</i> for Tap Major Diameter | |
|-----|--|--|---|--|---|--|
| 1 | 2 | 3 | 4 | 5 | 6 | |
| 20 | 0.0026 | 0.0052 | 0.010 | 0.010 | 0.0032 | |
| 18 | 0.0030 | 0.0060 | 0.011 | 0.011 | 0.0036 | |
| 16 | 0.0032 | 0.0064 | 0.011 | 0.011 | 0.0041 | |
| 14 | 0.0036 | 0.0072 | 0.008 | 0.012 | 0.0046 | |
| 13 | 0.0037 | 0.0074 | 0.008 | 0.012 | 0.0050 | |
| 12 | 0.0040 | 0.0080 | 0.009 | 0.013 | 0.0054 | |
| 11 | 0.0042 | 0.0084 | 0.010 | 0.013 | 0.0059 | |
| 10 | 0.0045 | 0.0090 | 0.011 | 0.014 | 0.0065 | |
| 9 | 0.0049 | 0.0098 | 0.012 | 0.014 | 0.0072 | |
| 8 | 0.0054 | 0.0108 | 0.014 | 0.015 | 0.0081 | |
| 7 | 0.0059 | 0.0118 | 0.015 | 0.015 | 0.0093 | |
| 6 | 0.0071 | 0.0142 | 0.018 | 0.018 | 0.0108 | |

NOTES:

- (1) National Class 3 pitch diameter tolerance from ASA B1.1-1960 (see p. 85).
- (2) Twice the NC-3 pitch diameter tolerance.
- (3) National Class 3 minor diameter tolerance from ASA B1.1-1960 (see p. 85).

| Nominal | Basic Major Diameter | | Basic Pitch Diameter | Basic Minor Diameter |
|-----------------|-------------------------|-----|-------------------------|--|
| Size | D bsc, d bsc | TPI | D_2 bsc, d_2 bsc | D ₁ bsc, d ₁ bsc |
| 1/4 | 0.2500 | 20 | 0.2175 | 0.1959 |
| 5/16 | 0.3125 | 18 | 0.2764 | 0.2524 |
| 3/8 | 0.3750 | 16 | 0.3344 | 0.3073 |
| 7/16 | 0.4375 | 14 | 0.3911 | 0.3602 |
| 1/2 | 0.5000 | 13 | 0.4500 | 0.4167 |
| 9/16 | 0.5625 | 12 | 0.5084 | 0.4723 |
| 5/8 | 0.6250 | 11 | 0.5660 | 0.5266 |
| 3/4 | 0.7500 | 10 | 0.6850 | 0.6417 |
| | | | | - N · |
| ⁷ /8 | 0.8750 | 9 | 0.8028 | 0.7547 |
| 1 | 1.0000 | 8 | 0.9188 | 0.8647 |
| 1 1/8 | 1.1250 | 7 | 1.0322 | 0.9704 |
| 11/4 | 1.2500 | 7 | 1.1572 | 1.0954 |
| 13/8 | 1.3750 | 6 | 1.2667 | 1.1946 |
| 1 1/2 | 1.5000 | 6 | 1.3917 | 1.3196 |

TABLE 4 BASIC DIMENSIONS FOR COARSE THREAD SERIES

8.1.1 External Thread Formulas for Limits of Size

- (a) (1) Maximum major diameter (d max.) for NC-5, HF equals basic major diameter (d bsc) minus allowrance from Table 2, column 2.
- (2) Maximum major diameter (d max.) for NC-5 CSF and NC-5 ONF equals basic major diameter (d bsc) minus allowance from Table 2, column 3
- (b) Minimum major diameter equals maximum major diameter (d max.) minus major diameter tolerance from Table 3, column 3.
- (c) Maximum pitch diameter (d_2 max.) for all materials equals basic pitch diameter (d_2 bsc) plus negative allowance from Table 2, column 6.
- (d) Minimum pitch diameter (d_2 min.) for all materials equals maximum pitch diameter (d_2 max.) minus pitch diameter tolerance from Table 3, column 2.
- (e) Maximum minor diameter (d_1 max.) equals maximum pitch diameter (d_2 max.) minus 0.66667H.
- (f) Minimum minor diameter $(d_1 \text{ min.})$ (reference only) equals minimum pitch diameter $(d_2 \text{ min.})$ minus 0.75H.

NOTE: This size is used in the design of tools. Acceptance of the minor diameter is by maximum material gage.

8.1.2 Internal Thread Formulas for Limits of Size

(a) Minimum major diameter (D min.) for all materials equals basic major diameter (D bsc) plus tolerance of 0.075H (Table 3, column 6). See Note in (b) below.

(b) Maximum major diameter (D max.) for all materials equals minimum major diameter (D min.) plus tolerance of 0.075H (Table 3, column 6).

NOTE: This size is used in the design of tools. Acceptance of the internal thread major diameter is by proper use of a maximum material GO thread gage.

- (c) Minimum pitch diameter (D_2 min.) for all materials equals basic pitch diameter (D_2 bsc) for UN-3B.
- (d) Maximum pitch diameter (D_2 max.) for all materials equals minimum pitch diameter (D_2 min.) plus pitch diameter tolerance from Table 3, column 2.
- (e) (1) Minimum minor diameter (D_1 min.) for NC-5 INF equals basic minor diameter (D_1 bsc).
- (2) Minimum minor diameter (D_1 min.) for NC-5 IF equals basic minor diameter (D_1 bsc) for sizes with more than 14 TPI. For 14 through 4 TPI use basic minor diameter (D_1 bsc) plus allowances tabulated in Table 2, column 4.
- (f) (I) Maximum minor diameter (D_1 max.) for NC-5 INF equals minimum minor diameter (D_1 min.) plus minor diameter tolerance from Table 3, column 5.
- (2) Maximum minor diameter (D_1 max.) for NC-5 IF equals minimum minor diameter (D_1 min.) plus minor diameter tolerance from Table 3, column 4.

9 THREAD CHARACTERISTICS

Tables 6, 7, and 8 are in compliance with the design and application data in Sections 8 and 10.

TABLE 5 THREAD CONSTANTS

| | D'ALL | ,, | 0.7504 | 0.666667 <i>H</i> | 0.5004 | 0.222224 | 27504 | 0.40000711 | 0.4511 | Truncation |
|-----|----------|----------|----------------|-------------------|----------------|-------------------|----------------|-------------------|---------------|------------|
| TPI | Pitch | Н | 0.750 <i>H</i> | U.00000/H | 0.500 <i>H</i> | 0.333333 <i>H</i> | 0.250 <i>H</i> | 0.166667 <i>H</i> | 0.15 <i>H</i> | [Note (1)] |
| 20 | 0.050000 | 0.043301 | 0.03248 | 0.02887 | 0.02165 | 0.01443 | 0.01083 | 0.00722 | 0.0065 | 0.00899 |
| 18 | 0.055556 | 0.048113 | 0.03608 | 0.03208 | 0.02406 | 0.01604 | 0.01203 | 0.00802 | 0.0072 | 0.00968 |
| 16 | 0.062500 | 0.054127 | 0.04060 | 0.03608 | 0.02706 | 0.01804 | 0.01353 | 0.00902 | 0.0081 | 0.01051 |
| 14 | 0.071429 | 0.061859 | 0.04639 | 0.04124 | 0.03093 | 0.02062 | 0.01546 | 0.01031 | 0.0093 | 0.01154 |
| | | | | | | 0, | | | | |
| 13 | 0.076923 | 0.066617 | 0.04996 | 0.04441 | 0.03331 | 0.02221 | 0.01665 | 0.01110 | 0.0100 | 0.01216 |
| 12 | 0.083333 | 0.072169 | 0.05413 | 0.04811 | 0.03608 | 0.02406 | 0.01804 | 0.01203 | 0.0108 | 0.01286 |
| 11 | 0.090909 | 0.078730 | 0.05905 | 0.05249 | 0.03936 | 0.02624 | 0.01968 | 0.01312 | 0.0118 | 0.01368 |
| 10 | 0.100000 | 0.086603 | 0.06495 | 0.05774 | 0.04330 | 0.02887 | 0.02165 | 0.01443 | 0.0130 | 0.01463 |
| | | | | | "O | | | | | |
| 9 | 0.111111 | 0.096225 | 0.07217 | 0.06415 | 0.04811 | 0.03207 | 0.02406 | 0.01604 | 0.0144 | 0.01576 |
| 8 | 0.125000 | 0.108253 | 0.08119 | 0.07217 | 0.05413 | 0.03608 | 0.02706 | 0.01804 | 0.0162 | 0.01712 |
| 7 | 0.142857 | 0.123718 | 0.09279 | 0.08248 | 0.06186 | 0.04124 | 0.03093 | 0.02062 | 0.0186 | 0.01882 |
| 6 | 0.166667 | 0.144338 | 0.10825 | 0.09623 | 0.07217 | 0.04811 | 0.03608 | 0.02406 | 0.0217 | 0.02100 |

(1) Truncation for maximum-material truncated setting plug gage equals $0.06\sqrt[3]{p^2} + 0.017p$.

9.1 Limits of Size

Limits of size for the national coarse series for 0.250 in. through 1.500 in. are given in Tables 6 and 7.

NOTE: Specifications for Class 5 Modified for K Monel external threads and usable for more materials are given in Appendix C.

9.2 Pitch Diameter Limits

- **9.2.1 External Thread.** One set of pitch diameter limits is maintained for each size regardless of material. The minimum pitch diameter on external threads is larger than the basic pitch diameter of comparable unified coarse threads.
- **9.2.2 Internal Thread.** One set of pitch diameter limits is maintained for each size regardless of material. The minimum pitch diameter on internal threads is the same as the basic pitch diameter of comparable unified coarse threads.

9.3 Major Diameter Limits

9.3.1 External Thread

- (a) The major diameter of the external thread is less than the basic major diameter, which is based on a truncation of H/8. This reduction provides a spiral eavity between the major diameters of the external thread and internal thread where the interference material can flow. (See para. 9.4.2.)
- (b) The hard ferrous materials and materials of similar hardness have a smaller major diameter than the soft ferrous and nonferrous materials.

9.3.2 Internal Thread ()

- (a) The minimum major diameter of the internal thread is equal to the minimum tap major diameter. [See para. 8.1.2(a).]
- (b) The maximum major diameter of the internal thread is nominally equal to the maximum major diameter of the tap. [See para. 8.1.2(b).]

9.4 Minor Diameter Limits

- **9.4.1 Internal Thread.** The internal thread minor diameter limits are National Class 3 for all sizes in nonferrous materials and for sizes 0.0250 in. through 0.375 in. for ferrous materials. For 0.4375 in. and larger sizes in ferrous materials, the minor diameters have been enlarged slightly in order to reduce driving torques.
- **9.4.2 External Thread.** The maximum minor diameter of the external thread is less than the basic minor

diameter. This provides a cavity between the external and internal thread minor diameters for additional interference material flow. (See para. 9.3.1.)

9.5 Other Screw Thread Characteristics

Tables 1 and 2 in ANSI/ASME B1.3M identify the external and internal product screw thread characteristic(s), respectively, which singly or cumulatively change both the maximum and minimum interference conditions.

9.6 Length of Engagement

For driving into copper alloys and ferrous materials, the length of engagement is 1.25D. For driving into other nonferrous materials, the length of engagement is 2.5D. These are tabulated in Table 8.

Tolerances for length of full-form external thread and for minimum depth of full-form internal thread in hole are provided because the assembled external thread shall not bottom nor shall the unfinished threads engage. False torque and excessive stress occur if one or both of the above conditions exist. (See Fig. 5.)

10 NOTES ON PRODUCT DESIGN AND APPLICATION

10.1 Conditions of Usage

The following are for plastic flow interference-fit conditions on which satisfactory application of products made to dimensions in Tables 6 and 7 are predicated. Deviations from the dimensions and application notes may result in unsatisfactory performance. In the manufacture or inspection of product threads, control and verification of the limits of size and the various individual thread elements, using measurement methods, ensure that the threads produced will be acceptable. (See Appendix B for information on elastic interference fit.)

10.2 External Threaded Products

- **10.2.1 Coated Parts.** Limits apply to bare or metallic coated parts.
- **10.2.2 Points.** Points of externally threaded products should be chamfered or otherwise reduced to a diameter below the minimum minor diameter of the thread.

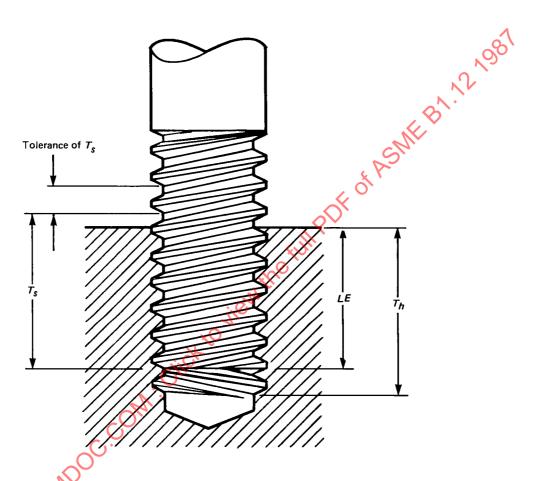


FIG. 5 ILLUSTRATION OF LE, T_s , TOLERANCE OF T_s , and T_h REQUIRED FOR ASSEMBLED THREADS (To Prevent Bottoming of Stud in Hole, See Table 8)

TABLE 6 EXTERNAL THREAD DIMENSIONS FOR CLASS 5 STANDARD (See Para. 10.2.3 for Application)

| | | | Major D | Diameter | | | ASM | | | |
|-----------------|---|---|---|---|--|--|--------|---------|---------|----------------|
| | Ferrous Ma Hardness C <i>LE</i> = 1 | or Driving in aterial With Over 160 HB 25 Diam. (1), (2)] | Brass an Material Wi 160 HE <i>LE</i> = 1. | or Driving in d Ferrous th Hardness d or Less 25 Diam. (1), (2)] | NC-5 ONF fo Nonferrou Except (Any Ha <i>LE</i> = 2. [Note | s Material : Brass irdness) 5 Diam. | o'' | iameter | Minor D | Diameter |
| Nominal Size | Max. | Min. | Max. | Min. | Max. | Min. | Max. | Min. | Max. | Min. (Ref.) |
| 0.2500-20 | 0.2470 | 0.2418 | 0.2470 | 0.2418 | 0.2470 | 0.2418 | 0.2230 | 0.2204 | 0.1932 | 0.1879 |
| 0.3125-18 | 0.3080 | 0.3020 | 0.3090 | 0.3030 | 0.3090 | 0.3030 | 0.2829 | 0.2799 | 0.2508 | 0.2438 |
| 0.3750-16 | 0.3690 | 0.3626 | 0.3710 | 0.3646 | 0.3710 | 0.3646 | 0.3414 | 0.3382 | 0.3053 | 0.2976 |
| 0.4375-14 | 0.4305 | 0.4233 | 0.4330 | 0.4258 | 0,4330 | 0.4258 | 0.3991 | 0.3955 | 0.3579 | 0.3491 |
| 0.5000-13 | 0.4920 | 0.4846 | 0.4950 | 0.4876 | 0.4950 | 0.4876 | 0.4584 | 0.4547 | 0.4140 | 0.4047 |
| 0.5625-12 | 0.5540 | 0.5460 | 0.5575 | 0.5495 | 0.5575 | 0.5495 | 0.5176 | 0.5136 | 0.4695 | 0.4595 |
| 0.6250-12 | 0.6140 | 0.6056 | 0.6195 | 0.6111 | 0.6195 | 0.6111 | 0.5758 | 0.5736 | 0.5233 | 0.4535 |
| 0.7500-10 | 0.7360 | 0.7270 | 0.7440 | 0.7350 | 0.7440 | 0.7350 | 0.6955 | 0.6910 | 0.6378 | 0.6260 |
| 0.8750- 9 | 0.8600 | 0.8502 | 0.8685 | 0.8587 | 0.8685 | 0.8587 | 0.8144 | 0.8095 | 0.7503 | 0.7373 |
| 1.0000- 8 | 0.9835 | 0.9727 | 0.9935 | 0.9827 | 0.9935 | 0.9827 | 0.9316 | 0.9262 | 0.8594 | 0.8450 |
| 1.1250- 7 | 1.1070 | 1.0952 | 1.1180 | 1.1062 | 1.1180 | 1.1062 | 1.0465 | 1.0406 | 0.9640 | 0.9478 |
| 1.2500- 7 | 1.2320 | 1.2200 | 1.2430 | 1.2312 | 1.2430 | 1.2312 | 1.1715 | 1.1656 | 1.0890 | 1.0728 |
| 1.3750- 6 | 1.3560 | 1.3410 | 1.3680 | 1.3538 | 1.3680 | 1.3538 | 1.2839 | 1.2768 | 1.1877 | 1.1685 |
| 1.5000- 6 | 1.4810 | 1.4670 | 1,4930 | 1.4788 | 1.4930 | 1.4788 | 1.4089 | 1.4018 | 1.3127 | 1.2935 |

NOTES:
(1) 160 HB is standard Brinell number using 10 mm ball and 3000 kgf. This is approximately equivalent to Rockwell hardness B83 (83 HRB).

⁽²⁾ See para. 9.6.

15

| | | NC-5 IF Ferrous Materia | | (See Para. 1 | L THREAD DIMENSIONS FOR CLAS (See Para. 10.2.3 for Application) NC-5 INF Nonferrous Material | | | DARD | | |
|-----------------|------------------------|----------------------------|--------------|------------------------|---|--------------|-----------------|--------|------------|-------------------------------|
| Nominal Size | Min. Minor Diam. | Max. Minor Diam. | Tap Drill | Min. Minor Diam. | Max. Minor Diam. | Tap Drill | Pitch D Min. | Max. | Major Min. | Diameter Max. [Note (1) |
| 0.2500-20 | 0.1960 | 0,2060 | 0.2031 | 0.1960 | 0.2060 | 0.2031 | 0.2175 | 0.2201 | 0.2532 | 0.2565 |
| 0.3125-18 | 0.2520 | 0.2630 | 0.2610 | 0.2520 | 0.2630 | 0.2610 | 0.2764 | 0.2794 | 0.3161 | 0.3197 |
| 0.3750-16 | 0.3070 | 0.3180 | 0.3160 | 0.3070 | 0.3180 | 0.3160 | 0.3344 | 0.3376 | 0.3790 | 0.3831 |
| 0.4375-14 | 0.3740 | 0.3810 | 0.3750 | 0.3600 | 0.3720 | 0.3680 | 0.3911 | 0.3947 | 0.4421 | 0.4468 |
| 0.5000-13 | 0.4310 | 0.4400 | 0.4331 | 0.4170 | 0.4290 | 0.4219 | 0.4500 | 0.4537 | 0.5050 | 0.5100 |
| 0.5625-12 | 0.4880 | 0.4970 | 0.4921 | 0.4720 | 0.4850 | 0.4844 | 0.5084 | 0.5124 | 0.5679 | 0.5733 |
| 0.6250-11 | 0.5440 | 0.5540 | 0.5469 | 0.5270 | 0.5400 | 0.5313 | 0.5660 | 0.5702 | 0.6309 | 0.6368 |
| 0.7500-10 | 0.6610 | 0.6780 | 0.6719 | 0.6420 | 0.6550 | 0.6496 | 0.6850 | 0.6895 | 0.7565 | 0.7630 |
| 0.8750- 9 | 0.7770 | 0.7890 | 0.7812 | 0.7550 | 0.7690 | 0.7656 | 0.8028 | 0.8077 | 0.8822 | 0.8894 |
| 1.0000- 8 | 0.8900 | 0.9040 | 0.8906 | 0.8650 | 0.8800 | 0.8750 | 0.9188 | 0.9242 | 1.0081 | 1.0162 |
| 1.1250- 7 | 1.0000 | 1.0150 | 1.0000 | 0.9700 | 0.9860 | 0.9844 | 1.0322 | 1.0381 | 1.1343 | 1.1436 |
| 1.2500- 7 | 1.1250 | 1.1400 | 1.1250 | 1,0950 | 1.1110 | 1.1094 | 1.1572 | 1.1631 | 1.2593 | 1.2686 |
| 1.3750- 6 | 1.2290 | 1.2470 | 1.2344 | 1,1950 | 1.2130 | 1.2031 | 1.2667 | 1.2738 | 1.3858 | 1.3967 |
| 1.5000- 6 | 1.3540 | 1.3720 | 1.3594 | <u>-</u> 1.3200 | 1.3380 | 1.3281 | 1.3917 | 1.3988 | 1.5108 | 1.5217 |

NOTE:
(1) Reference, maximum major diameter of tap.

TABLE 8 INTERFERENCES, ENGAGEMENT LENGTHS, AND TORQUES FOR CLASS 5 STANDARD (See Para. 10.2.3 for Application)

| | | | Enga | Torque at 1.25 <i>D</i> | | | | | | |
|-----------------|------------------------------------|--------|----------------------|---|---------------------------------|----------------------|-------------------------------------|---------------------------------|----------------|----------------|
| | Interferences on Pitch Diameter | | In B | In Brass and Ferrous Material | | | In Nonferrous Material Except Brass | | | |
| Nominal Size | Max. | Min. | <i>LE</i> [Note (2)] | <i>T_s</i> [Note (3)] | <i>T_h</i> [Note (4)] | <i>LE</i> [Note (2)] | [Note (3)] | <i>T_h</i> [Note (4)] | Max., lb-ft | Min., lb-ft |
| 0.2500-20 | 0.0055 | 0.0003 | 0.312 | 0.375 ^{+0.125} -0.000 | 0.375 | 0.625 | 0.688 +0.125 -0.000 | 0.688 | 12 | 3 |
| 0.3125-18 | 0.0065 | 0.0005 | 0.391 | 0.469 ^{+0.139} -0.000 | 0.469 | 0.781 | 0.859 ^{+0.139} -0.000 | 0.859 | 19 | 6 |
| 0.3750-16 | 0.0070 | 0.0Ó06 | 0.469 | $0.562 \begin{array}{l} +0.156 \\ -0.000 \end{array}$ | 0.562 | 0.938 | 1.031 ^{+0.156} -0.000 | 1.031 | 35 | 10 |
| 0.4375-14 | 0.0080 | 0.0008 | 0.547 | 0.656 ^{+0.179} -0.000 | 0.656 | 1.094 | 1.203 ^{+0.179} -0.000 | 1.203 | 45 | 15 |
| 0.5000-13 | 0.0084 | 0.0010 | 0.625 | 0.750 ^{+0.192} -0.000 | 0.750 | 1.250 | 1.375 ^{+0.192} -0.000 | 1.375 | 75 | 20 |
| 0.5625-12 | 0.0092 | 0.0012 | 0.703 | 0.844 +0.208 | 0.844 | 1.406 | 1.547 ^{+0.208} -0.000 | 1.547 | 90 | 30 |
| 0.6250-11 | 0.0098 | 0.0014 | 0.781 | +0.227 -0.000 | 0.938 | 1.562 | 1.719 ^{+0.227} -0.000 | 1.719 | 120 | 37 |
| 0.7500-10 | 0.0105 | 0.0015 | 0.938 | 1.125 ^{+0.250} -0.000 | 1.125 | 1.875 | 2.062 +0.250 -0.000 | 2.062 | 190 | 60 |
| 0.8750- 9 | 0.0116 | 0.0018 | 0.094 | 1.312 ^{+0.278} -0.000 | 1.312 | 2.188 | 2.406 +0.278 -0.000 | 2.406 | 250 | 90 |
| 1.0000- 8 | 0.0128 | 0.0020 | 1.250 | 1.500 ^{+0.312} -0.000 | 1.500 | 2.500 | 2.750 +0.312 -0.000 | 2.750 | 400 | 125 |
| 1.1250- 7 | 0.0143 | 0.0025 | 1.406 | 1.688 +0.357 -0.000 | 1.688 | 2.812 | 3.094 +0.357 -0.000 | 3.094 | 470 | 155 |

TABLE 8 INTERFERENCES, ENGAGEMENT LENGTHS, AND TORQUES FOR CLASS STANDARD (CONT'D) (See Para. 10.2.3 for Application)

| | | | | Enga | pths | Torque at 1.25 <i>D</i> | | | | | |
|--|-----------------|------------------------------------|--------|----------------------|-----------------------------------|-----------------------------------|------------|---------------------------------|---------------------------------|----------------|----------------|
| | | Interferences on Pitch Diameter | | In B | rass and Ferrous Ma | terial | In Nont | Engagement, Ferrous Material | | | |
| | Nominal Size | Max. | Min. | <i>LE</i> [Note (2)] | <i>T_s</i> [Note (3)] | · <i>T_h</i> [Note (4)] | [Note (2)] | <i>T_s</i> [Note (3)] | <i>T_h</i> [Note (4)] | Max., lb-ft | Min., lb-ft |
| | 1.2500- 7 | 0.0143 | 0.0025 | 1.562 | 1.875 +0.357 -0.000 | 1.875 N | 3.125 | 3.438 +0.357 -0.000 | 3.438 | 580 | 210 |
| | 1.3750- 6 | 0.0172 | 0.0030 | 1.719 | 2.062 ^{+0.419} -0.000 | 2.062 | 3.438 | 3.781 +0.419 -0.000 | 3.781 | 705 | 250 |
| | 1.5000- 6 | 0.0172 | 0.0030 | 1.875 | 2.250 ^{+0.419} -0.000 | 2.250 | 3.750 | 4.125 +0.419 -0.000 | 4.125 | 840 | 325 |

NOTES:

- (1) See Fig. 5.
- (2) LE = length of engagement
- (3) $T_s = \text{external thread length of full-form thread}$ (4) $T_h = \text{minimum depth of full-form thread in hole}$

- 10.2.3 Materials of Externally Threaded Ferrous Products. The length of engagement, depth of thread engagement, and pitch diameter in Tables 6 through 8 are designed to produce adequate torque conditions when heat-treated medium-carbon steel products, ASTM A 325 (SAE Grade 5) or better, i.e., minimum ultimate tensile strength of 145,000 psi, are used. In many applications, case-carburized products and nonheat-treated medium-carbon steel products, SAE Grade 4, are satisfactory. SAE Grades 1 and 2 may be usable under certain conditions. This Standard is not intended to cover the use of externally threaded products made of stainless steel, silicon bronze, brass, or similar materials. Where such materials are used, the dimensions listed herein will probably require adjustment based on pilot experimental work with the combination or materials involved.
- **10.2.4 Metal Flow.** Metal flows into the major diameter cavity when hard studs are assembled into hard internal threads.
- **10.2.5 Cleanliness.** Threads should be free from nicks, burrs, chips, grit, or other extraneous material before applying necessary lubricant and driving.

10.3 Internal Threaded Products

- 10.3.1 Countersinks. Holes should be countersunk to a diameter greater than the major diameter in order to facilitate starting of the externally threaded product and to prevent raising a lip around the hole after driving due to insufficient cavity space at major diameter.
- 10.3.2 Taper. Internal tapered threads with smaller diameter at the entering end tend to break loose when stud is started.
- 10.3.3 Metal Flow. Metal flows into the minor diameter cavity when hard external threads are assembled into soft internal threads.
- 10.3.4 Cleanliness. Holes should be free from nicks, burrs, chips, grit, or other foreign material before driving studs or screws.

10.4 Lead and Angle Variations

The lead variation values tabulated in Table 9 are the maximum variations from specified lead between any two points not farther apart than the length of the standard GO thread gage. Flank angle variation values tabulated in Table 10 are maximum variations from the basic 30 deg. angle between thread flanks and perpendiculars to the thread axis.

- 10.4.1 Stress on Thread Flank. Lead variation does not change the volume of displaced metal, but it exerts a cumulative unilateral stress on the pressure side of the thread flank. For a ½-20 thread assembly at maximum-material condition with a lead variation equivalent to one-half of the pitch diameter tolerance, an additional 8% of the displaced metal is forced onto the pressure flanks. For 1½-6 threads, the figure is 5%.
- 10.4.2 Control. Control of the difference between pitch diameter size and functional diameter size to within one-half the pitch diameter tolerance will hold lead and angle variables to within satisfactory limits. Both of the variations may produce unacceptable torque and faulty assemblies. (See para 11.2.2.)

10.5 Cavity Space for Interference Material

Calculations show that for the three small sizes of ferrous and all sizes of nonferrous material, cavity spaces at maximum interference are far less than the volumes of the interference metal displaced. When there is not sufficient reservoir for the escape of interference material, the probability of assembly failure is higher. (See Appendix D, Section D2.)

For consistency in assembly, selection of mating parts within the tolerance ranges to provide less interference may be necessary so that more space is available.

10.6 Thread Axis Position

A perfect thread has a common axis for the major diameter cylinder, the minor diameter cylinder, and the pitch diameter cylinder. Interference-fit thread assemblies of imperfect threads may have three axes either parallel or skew to each other, resulting in erratic torquing, excessive unilateral stress, nonuniform change in interference metal during assembly, and uneven available cavity space for metal to flow into, even though the interference metal displaced remains the same.

The circular runout (full-indicator movement) of the pitch and crest diameters over the thread length shall not exceed one-half the pitch diameter tolerance for the external or internal threaded products.

10.7 Surface Roughness

Surface roughness is not a required measurement. Roughness between 63 μ in. and 125 μ in. Ra is recommended. Surface roughness greater than 125 μ in. Ra may encourage galling and tearing of threads. Surfaces with roughness less than 63 μ in. Ra may hold insufficient lubricant and wring or weld together.

TABLE 9 MAXIMUM ALLOWABLE VARIATIONS IN LEAD AND MAXIMUM EQUIVALENT CHANGE IN FUNCTIONAL DIAMETER (See Para. 10.4 and Section 11 for Application)

| | External and Internal Threads | | | | | |
|-----------------|--|--|--|--|--|--|
| Nominal Size | Allowable Variation in Axial Lead (Plus or Minus) | Maximum Equivalent Change in Functional Diameter (Plus for External, Minus for Internal) | | | | |
| 0.2500-20 | 0.0008 | 0.0013 | | | | |
| 0.3125-18 | 0.0009 | 0.0015 | | | | |
| 0.3750-16 | 0.0009 | 0.0016 | | | | |
| 0.4375-14 | 0.0009 0.0009 0.0010 0.0011 0.0012 0.0012 | 0.0018 | | | | |
| 0.5000-13 | 0.0011 | 0.0018 | | | | |
| 0.5625-12 | 0.0012 | 0.0020 | | | | |
| 0.6250-11 | 0.0012 | 0.0021 | | | | |
| 0.7500-10 | 0.0013 | 0.0022 | | | | |
| 0.8750- 9 | 0.0014 | 0.0024 | | | | |
| 1.0000- 8 | 0.0016 | 0.0027 | | | | |
| 1.1250- 7 | 0.0017 | 0.0030 | | | | |
| 1.2500- 7 | 0.0017 | 0.0030 | | | | |
| 1.3750- 6 | 0.0020 | 0.0036 | | | | |
| 1.5000- 6 | 0.0020 | 0.0036 | | | | |

GENERAL NOTE:

GENERAL NOTE:

The equivalent change in functional diameter applies to total effect of form errors. (See para. 10.4.2.) Maximum allowable variation in lead is permitted only when all other form variations are zero. For sizes not tabulated, maximum allowable variation in lead is equal to 0.57735 times onehalf the pitch diameter tolerance.

TABLE 10 MAXIMUM ALLOWABLE VARIATION IN 30 deg. BASIC HALF-ANGLE OF EXTERNAL AND INTERNAL SCREW THREADS

(See Paras. 11.1.2, 11.1.3, 11.1.4, and 11.2.2 for Application)

| TPI | in Half-Ang (Plus o | e Variation gle of Thread Minus), and min | |
|-------|------------------------|--|---------|
| 32 | 1 | 30 | |
| 28 | 1 | 20 | |
| 27 | 1 | 20 | |
| 24 | 1 | 15 | |
| 20 | 1 | 10 | |
| 18 | 1 | 05 | |
| 16 | 1 | 00 | |
| 14 | 0 | 55 | |
| 13 | 0 | 55 | |
| 12 | 0 | 50 | |
| 111/2 | 0 | 50 | |
| 11 | 0 | 50 | |
| 10 | 0 | 50 | |
| 9 | 0 | 50 | |
| 8 | 0 | 45 | . 0 |
| 7 | 0 | 45 | The |
| . 6 | 0 | 40 | to jiel |
| 5 | 0 | 40 | |
| 41/2 | 0 | 40 | |
| 4 | 0 | 40 | |

10.8 Lubrication

10.8.1 Ferrous Material. For driving in ferrous material, an appropriate lubricant must be used particularly in the hole (and it may also be applied to the male members). A noncarbonized type of lubricant (such as a rubber-in-water dispersion) is suggested. Some other lubricants are petrolatum with graphite, molybdenum disulfide, isopropyl alcohol with graphite, and white lead in oil. In applying it to the hole, care must be taken so that an excess amount of lubricant will not cause the male member to be impeded by hydraulic pressure in a blind hole.

10.8.2 Nonferrous Material. When Class 5 threaded products are driven in nonferrous material, lubrication may not be needed. The use of medium gear oil for driving in aluminum is recommended. American

research has observed that the minor diameter of lubricated tapped holes in nonferrous materials may tend to close in, i.e., be reduced in driving, whereas with an unlubricated hole the minor diameter may tend to open up in some cases.

10.8.3 Sealant. Where sealing is involved, a lubricant should be selected which is insoluble in the medium being sealed.

10.9 Driving Speed

This Standard makes no recommendation for driving speed. Some opinion has been advanced that careful selection and control of driving speed is desirable to obtain optimum results with various combinations of surface hardness and roughness. Applications may indicate what limitations should be placed on driving speeds. When excessive heat is being generated during assembly, stopping to let heat dissipate may be advisable in some applications.

10.10 Relation of Driving Torque to Length of Engagement

Torque increases as the length of engagement increases. Torque increase is proportionately more rapid as size increases.

Industrial research around 1952 showed for the higher interference conditions that the direct increase in torque per turn leveled off after the assembly was well advanced. The intense heat generated during continuous assembly by forced metal movement may be sufficient to soften the metal being displaced into the designed cavity space. Failure during assembly or even in breakaway may be the result of the assembly welding together.

10.11 Breakloose Torques

This Standard does not establish recommended breakloose torques.

11 PRODUCT SCREW THREAD ACCEPTABILITY

11.1 Gaging Systems

Screw thread gaging systems for dimensional acceptability are selected in accordance with ANSI/ASME B1.3M.

The design concept for interference-fit thread assemblies does not lend itself to control of functional diameter size only.

- 11.1.1 System 21. When System 21 of ANSI/ASME B1.3M is selected, product thread lead (including helix), flank angle variations, and circular runout are not considered. Where there is assembly and performance concern for uniform thickness of interference metal, cavity space, prevailing torque, and uniform stress, System 21 alone may not be acceptable, since it does not provide for minimum-material size control.
- 11.1.2 System 22. When System 22 of ANSI/ASME B1.3M is selected, pitch diameter or thread-groove diameter inspection is required, and the product thread lead (including helix) and flank angles shall be considered acceptable when the minimum-material size (pitch diameter or thread-groove diameter in ANSI/ASME B1.3M) and the maximum-material size (GO in ANSI/ASME B1.3M) are accepted by the gages specified for System 22, over the standard GO thread gage length.
- ASME B1.3M is selected, pitch diameter or thread-groove diameter inspection is required, and the product thread lead (including helix) and flank angles shall be considered acceptable if they are within the allowable variations, specified in Tables 9 and 10, respectively. Also, the minimum-material size (pitch diameter or thread-groove diameter in ANSI/ASME B1.3M) and maximum-material size (GO in ANSI/ASME B1.3M) must be accepted by the gages specified for System 23, over the standard GO thread gage length.

Allowable variations in lead and flank angles are maximum values. Maximum variation in each of these and pitch diameter folerance cannot be taken simultaneously. (See paras. 10.4.2 and 11.2.2.)

11.1.4 Modified System. When individual inspections of lead (including helix) and flank angle variations are required, in addition to System 21 or 22 of ANSI/ASME B1.3M, the allowable variations for these characteristics shall be specified.

- 11.2 Product Thread Characteristics
 Conformance Requirements Over Length
 of Engagement for Gaging Systems 22
 and 23
- 11.2.1 Diameter Size—Pitch Diameter, Functional Diameter Size, Major Diameter, Minor Diameter. Functional diameter size measurement verifies the maximum-material size over the gaging length. Pitch diameter size measurements at positions along and around the product thread verify the minimum-material size. Taper and roundness are included in the pitch diameter size measurements; therefore, they may not exceed the pitch diameter size limits. See para. 10.3.2.) Major diameter and minor diameter size verifies the cavity space. Table 11 gives limits of size for working gages and Table 12 gives limits of size for setting gages. Table 5 lists constants used in preparing gage dimension.
- 11.2.2 Form Lead, Flank Angle, Root Profile, Crest Profile. When specified by the gaging system, lead and flank angles are measured directly or as pitch diameter equivalents. Cumulative form restrictions in para, 10.4.2 apply. Root and crest profile are verified by optical projection or a mechanical/electrical tracer when specified.
- 11.2.3 Position of Axes When Assembled. The independent measurements of the various screw-thread characteristics do not ensure the required coaxial relationship of the internal and external threads at assembly. When circular runout inspection is specified, refer to para. 10.6 for tolerances.

12 TORQUE

The maximum and minimum torque values were established by the National Screw Thread Commission in 1925 from data submitted from many companies. They plotted the volume of interference material per turn against the tangential force at the thread surface and developed a parabolic equation.

$$F^2 = 9 \times 10^8 V$$
 for maximum torque

where

 $V = \text{volume of interference material per turn, in.}^3$

F = tangential forces per turn at thread surface, lb

TABLE 11 WORKING GAGES¹

| - Ilandin - Ilan | Gages for External Threads | | | | | | | Gages for Internal Threads | | | | | |
|--|----------------------------|--------|------------------|----------------------------------|---------------|---------------|------------------------------|----------------------------|-----------------|---------------|----------------|----------------------------------|---------------|
| | X Thread Gages | | | | | | X Thread Gages | | | | | | |
| | Max. Material Mir | | Min. M | Z Plain G Min. Material Major | | · 1 | | Max. Material | | Min. Material | | Z Plain Gages for Minor Diam. | |
| Nominal Size and Designation | Pitch Diam. | | | Minor Diam. | Max. Matl. | Min. Matl. | Nominal Size and Designation | Major Pitch Diam Diam. | | | Pitch Diam. | | Min. Matl. |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | \(\) 9 | 10 | 11 | 12 | 13 | 14 |
| 1/4-20 NC-5 HF, | 0.2230 | 0.2014 | 0.2204 | 0.2096 | 0.2470 | 0.2418 | 1/4-20 NC-5 IF, | 0.2500 | 0.21 7 5 | 0.2418 | 0.2201 | 0.1960 | 0.2060 |
| NC-5 CSF, | 0.2227 | 0.2009 | 0.2207 | 0.2101 | 0.2469 | 0.2419 | NC-5 INF | 0.2505 | 0.2178 | .0.2413 | 0.2198 | 0.1961 | 0.2059 |
| NC-5 ONF | | | | | | | (1). | | | | | | |
| 5/16-18 NC-5 HF | 0.2829 | 0.2588 | 0.2799 | 0.2679 | 0.3080 | 0.3020 | 5/16-18 NC-5 IF, | 0.3125 | 0.2764 | 0.3035 | 0.2794 | 0.2520 | 0.2630 |
| 710 10 110 0 111 | 0.2826 | 0.2583 | 0.2802 | 0.2684 | 0.3079 | 0.3021 | | 0.3130 | 0.2767 | 0.3030 | 0.2791 | 0.2521 | 0.2629 |
| 5/16-18 NC-5 CSF, | 0.2829 | 0.2588 | 0.2799 | 0.2679 | 0.3090 | 0.3030 | NC-5 INF | | | | | | |
| NC-5 ONF | 0.2826 | 0.2583 | 0.2802 | 0.2684 | 0.3089 | 0.3031 | The | · | | | | | |
| 3/8-16 NC-5 HF | 0.3414 | 0.3143 | 0.3382 | 0.3247 | 0.3690 | 0.3626 | 3/8-16 NC-5 IF. | 0.3750 | 0.3344 | 0.3647 | 0.3376 | 0.3070 | 0.3180 |
| %-10 NC-5 HF | 0.3414 | 0.3143 | 0.3385 | 0.3253 | 0.3689 | 0.3627 | NC-5 INF | 0.3756 | 0.3347 | 0.3641 | 0.3373 | 0.3071 | 0.3179 |
| 3/8-16 NC-5 CSF, | 0.3414 | 0.3137 | 0.3382 | 0.3247 | 0.3710 | 0.3646 | 1100 | 0.0.0 | | | | | |
| NC-5 ONF | 0.3411 | 0.3137 | 0.3385 | 0.3253 | 0.3709 | 0.3647 | | | | | | | |
| 110 0 0111 | 0.0 | 0.0.07 | 0.000 | | 1. | | | - | | | <i>'</i> | | |
| 7/18-14 NC-5 HF | 0.3991 | 0.3682 | 0.3955 | 0.3800 | 0.4305 | 0.4233 | 7/16-14 NC-5 IF | 0.4375 | 0.3911 | 0.4256 | 0.3947 | 0.3740 | 0.3810 |
| | 0.3988 | 0.3676 | 0.3958 | 0.3806 | 0.4304 | 0.4234 | | 0.4381 | 0.3914 | 0.4250 | 0.3944 | 0.3741 | 0.3809 |
| 7/16-14 NC-5 CSF, | 0.3991 | 0.3682 | 0.3955 | 0.3800 | 0.4330 | 0.4258 | 7/16-14 NC-5 INF | 0.4375 | 0.3911 | 0.4256 | 0.3947 | 0.3600 | 0.3720 |
| NC-5 ONF | 0.3988 | 0.3676 | 0.3958 | 0.3806 | 0.4329 | 0.4259 | | 0.4381 | 0.3914 | 0.4250 | 0.3944 | 0.3601 | 0.3719 |
| 1/2-13 NC-5 HF | 0.4584 | 0.4251 | 0.4547 | 0.4380 | 0.4920 | 0.4846 | 1/2-13 NC-5 IF | 0.5000 | 0.4500 | 0.4870 | 0.4537 | 0.4310 | 0.4400 |
| 72-13 10-3111 | 0.4581 | 0.4245 | 0.4550 | 0.4386 | 0.4919 | 0.4847 | | 0.5006 | 0.4503 | 0.4864 | 0.4534 | 0.4311 | 0.4399 |
| 1/2-13 NC-5 CSF, | 0.4584 | 0.4251 | 0.4547 | 0.4380 | 0.4950 | 0.4876 | 1/2-13 NC-5 INF | 0.5000 | 0.4500 | 0.4870 | 0.4537 | 0.4170 | 0.4290 |
| NC-5 ONF | 0.4581 | 0.4245 | 0.4550 | 0.4386 | 0.4949 | 0.4877 | | 0.5006 | 0.4503 | 0.4864 | 0.4534 | 0.4171 | 0.4289 |
| % 40 NO 5 U5 | 0.5470 | 0.404 | 0.5400 | 0.4056 | 0.5540 | 0.5460 | %16-12 NC-5 IF | 0.5625 | 0.5084 | 0.5485 | 0.5124 | 0.4880 | 0.4970 |
| %16-12 NC-5 HF | 0.5176 | 0.4815 | 0.5136 0.5139 | 0.4956 0.4962 | 0.5540 | 0.5460 | 716-12 NC-5 IF | 0.5623 | 0.5084 | 0.5479 | 0.5121 | 0.4881 | 0.4969 |
| %16-12 NC-5 CSF, | 0.5173 | 0.4809 | 0.5139 | 0.4962 | 0.5539 | 0.5495 | %16-12 NC-5 INF | 0.5625 | 0.5084 | 0.5485 | 0.5124 | 0.4720 | 0.4850 |
| %16-12 NC-5 CSF, NC-5 ONF | 0.5176 | 0.4809 | 0.5136 | 0.4962 | 0.5574 | 0.5496 | /16-12 NO-3 IN | 0.5631 | 0.5087 | 0.5479 | 0.5121 | 0.4721 | 0.4849 |
| INC-5 OINF | 0.5173 | 0.4609 | 0.5139 | 0.4302 | 0.5574 | 3.5450 | | 0.0001 | 2.5557 | | | | |

TABLE 11 WORKING GAGES¹ (CONT'D)

| | | Ga | ges for Ext | ernal Threa | ads | | | | Ga | ges for Int | ernal Threa | ads | |
|------------------------------|----------------|----------------|----------------|----------------|--------------------|--------------------|---------------------------------|----------------|----------------|----------------|----------------|---------------|----------------|
| | | X Threa | d Gages | | | | | | X Threa | d Gages | 20. | | |
| | Max. N | /laterial | Min. N | laterial | Z Plain (Major | Sages for Diam. | , | Max. N | Vaterial | Min. N | laterial | | ages for Diam. |
| Nominal Size and Designation | Pitch Diam. | Minor Diam. | Pitch Diam. | Minor Diam. | Max. Matl. | Min. Mati. | Nominal Size and Designation | Major Diam. | Pitch Diam. | Major Diam. | Pitch Diam. | Max. Matl. | Min. Matl. |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 |
| %-11 NC-5 HF | 0.5758 | 0.5364 | 0.5716 | 0.5519 | 0.6140 | 0.6056 | %-11 NC-5 IF | 0.6250 | 0.5660 | 0.6096 | 0.5702 | 0.5440 | 0.5540 |
| | 0.5755 | 0.5358 | 0.5719 | 0.5525 | 0.6139 | 0.6057 | | 0.6256 | 0.5663 | 0.6090 | 0.5699 | 0.5441 | 0.5539 |
| %-11 NC-5 CSF, | 0.5758 | 0.5364 | 0.5716 | 0.5519 | 0.6195 | 0.6111 | %-11 NC-5 INF _ | 0.6250 | 0.5660 | 0.6096 | 0.5702 | 0.5270 | 0.5400 |
| NC-5 ONF | 0.5755 | 0.5358 | 0.5719 | 0.5525 | 0.6194 | 0.6112 | . ? ` | 0.6256 | 0.5663 | 0.6090 | 0.5699 | 0.5271 | 0.5399 |
| 3/4-10 NC-5 HF | 0.6955 | 0.6522 | 0.6910 | 0.6694 | 0.7360 | 0.7270 | 3/4-10 NC-5 IF | 0.7500 | 0.6850 | 0.7328 | 0.6895 | 0.6610 | 0.6780 |
| 74 10 110 0 111 | 0.6952 | 0.6516 | 0.6913 | 0.6700 | 0.7359 | 0.7271 | 74 10 110 00 | 0.7506 | 0.6853 | 0.7322 | 0.6892 | 0.6611 | 0.6779 |
| 3/4-10 NC-5 CSF, | 0.6955 | 0.6522 | 0.6910 | 0.6694 | 0.7440 | 0.7350 | 3/4-10 NC-5 INF | 0.7500 | 0.6850 | 0.7328 | 0.6895 | 0.6420 | 0.6550 |
| NC-5 ONF | 0.6952 | 0.6516 | 0.6913 | 0.6700 | 0.7439 | 0.7351 | 1, 0,100 | 0.7506 | 0.6853 | 0.7322 | 0.6892 | 0.6421 | 0.6549 |
| | | | | | | | W W | | | | | | |
| %- 9 NC-5 HF | 0.8144 | 0.7663 | 0.8095 | 0.7854 | 0.8600 | 0.8502 | %- 9 NC-5 IF | 0.8750 | 0.8028 | 0.8558 | 0.8077 | 0.7770 | 0.7890 |
| | 0.8141 | 0.7656 | 0.8098 | 0.7861 | 0.8599 | 0.8503 | 4 | 0.8757 | 0.8031 | 0.8551 | 0.8074 | 0.7771 | 0.7889 |
| %- 9 NC-5 CSF, | 0.8144 | 0.7663 | 0.8095 | 0.7854 | 0.8685 | 0.8587 | ⁷ /8- 9 NC-5 INF | 0.8750 | 0.8028 | 0.8558 | 0.8077 | 0.7550 | 0.7690 |
| NC-5 ONF | 0.8141 | 0.7656 | 0.8098 | 0.7861 | 0.8684 | 0.8588 | | 0.8757 | 0.8031 | 0.8551 | 0.8074 | 0.7551 | 0.7689 |
| | | | | | <i>~</i> | | | | | | | | |
| 1 - 8 NC-5 HF | 0.9316 | 0.8775 | 0.9262 | 0.8991 | 0.9835 | 0.9727 | 1 - 8 NC-5 IF | 1.0000 | 0.9188 | 0.9783 | 0.9242 | 0.8900 | 0.9040 |
| | 0.9312 | 0.8768 | 0.9266 | 0.8998 | 0.9834 | 0.9728 | | 1.0007 | 0.9192 | 0.9776 | 0.9238 | 0.8901 | 0.9039 |
| 1 - 8 NC-5 CSF, | 0.9316 | 0.8775 | 0.9262 | 0.8991 | 0.9935 | 0.9827 | 1 - 8 NC-5 INF | 1.0000 | 0.9188 | 0.9783 | 0.9242 | 0.8650 | 0.8800 |
| NC-5 ONF | 0.9312 | 0.8768 | 0.9266 | 0.8998 | 0.9934 | 0.9828 | | 1.0007 | 0.9192 | 0.9776 | 0.9238 | 0.8651 | 0.8799 |
| 11/8- 7 NC-5 HF | 1.0465 | 0.9846 | 1.0406 | 1.0097 | 1.1070 | 1.0952 | 11/8- 7 NC-5 IF | 1.1250 | 1.0322 | 1.1000 | 1.0381 | 1.0000 | 1.0150 |
| | 1.0461 | 0.9839 | 1.0410 | 1.0104 | 1.1069 | 1.0953 | | 1.1257 | 1.0326 | 1.0993 | 1.0377 | 1.0001 | 1.0149 |
| 11/8- 7 NC-5 CSF, | 1.0465 | 0.9846 | 1.0406 | 1.0097 | 1.1180 | 1.1062 | 11/8- 7 NC-5 INF | 1.1250 | 1.0322 | 1.1000 | 1.0381 | 0.9700 | 0.9860 |
| NC-5 ONF | 1.0461 | 0.9839 | 1.0410 | 1.0104 | 1.1179 | 1.1063 | | 1.1257 | 1.0326 | 1.0993 | 1.0377 | 0.9701 | 0.9859 |
| | | | 57 | | | | | | | | | | |
| 11/4- 7 NC-5 HF | 1.1715 | 1.1096 | 1.1656 | 1.1347 | 1.2320 | 1.2200 | 11/4- 7 NC-5 IF | 1.2500 | 1.1572 | 1.2250 | 1.1631 | 1.1250 | 1.1400 |
| | 1.1711 | 1.1089 | 1.1660 | 1.1354 | 1.2319 | 1.2201 | | 1.2507 | 1.1576 | 1.2243 | 1.1627 | 1.1251 | 1.1399 |
| 11/4- 7 NC-5 CSF, | 1.1715 | 1.1096 | 1.1656 | 1.1347 | 1.2430 | 1.2312 | 11/4- 7 NC-5 INF | 1.2500 | 1.1572 | 1.2250 | 1.1631 | 1.0950 | 1.1110 |
| NC-5 ONF | 1.1711 | 1.1089 | 1.1660 | 1.1354 | 1.2429 | 1.2313 | | 1.2507 | 1.1576 | 1.2243 | 1.1627 | 1.0951 | 1.1109 |
| | | ~S. | | | | l | | | l | | | | |

TABLE 11 WORKING GAGES¹ (CONT'D)

| | | Ga | ges for Ext | ernal Threa | ads | | | , 01 | Ga | ges for Int | ernal Threa | ads | |
|------------------------------|--------------------------|------------------|------------------|------------------|--------------------------|-------------------|------------------------------|------------------|------------------|------------------|------------------|------------------|-------------------|
| | | X Threa | d Gages | | | | | X | X Threa | d Gages | | | |
| | Max. N | /laterial | Min. N | laterial | Z Plain G Major | ages for Diam. | Fuller | Max. N | /laterial | Min. N | laterial | | ages for Diam. |
| Nominal Size and Designation | Pitch Diam. | Minor Diam. | Pitch Diam. | Minor Diam. | Max. Matl. | Min. Mati. | Nominal Size and Designation | Major Diam. | Pitch Diam. | Major Diam. | Pitch Diam. | Max. Matl. | Min. Matl. |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 |
| 13%- 6 NC-5 HF | 1.2839 1.2835 | 1.2117 | 1.2768 | 1.2407 1.2415 | 1.3560 1.3559 | 1.3410 1.3411 | 1%- 6 NC-5 IF | 1.3750 1.3758 | 1.2667 1.2671 | 1.3460 1.3452 | 1.2738 | 1.2290 1.2291 | 1.2470 |
| 1%- 6 NC-5 CSF, NC-5 ONF | 1.2839 1.2835 | 1.2117 | 1.2768 1.2772 | 1.2407 | 1.3680 1.367 9 | 1.3538 1.3539 | 13/8- 6 NC-5 INF | 1.3750 1.3758 | 1.2667 1.2671 | 1.3460 1.3452 | 1.2738 1.2734 | 1.1950 1.1951 | 1.2130 1.2129 |
| 1½- 6 NC-5 HF | 1.4089 | 1.3367 1.3359 | 1.4018 | 1.3657 1.3665 | 1.4810 | 1.4670 1.4671 | 1½- 6 NC-5 IF | 1.5000 1.5008 | 1.3917 | 1.4710 1.4702 | 1.3988 | 1.3540 | 1.3720 |
| 1½- 6 NC-5 CSF, NC-5 ONF | 1.4089 1.408 5 | 1.3367 1.3359 | 1.4018 1.4022 | 1.3657 1.3665 | 1.4930 | 1.4788 1.4789 | 1½- 6 NC-5 INF | 1.5000 1.5008 | 1.3917 1.3921 | 1.4710 1.4702 | 1.3988 1.3984 | 1.3200 1.3201 | 1.3380 |

NOTE:
(1) For HF, CSF, and ONF, and for IF and INF, the respective thread gages are the same. The plain gages are not interchangeable.

TABLE 12 SETTING GAGES

| | | | W Thread-S | etting Plugs | | | | | | |
|--------------------------------------|-------------------------|-------------------------|------------------------------|-------------------------|-------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| | | Max. Material | | | Min. Material | | | W Thread-S | etting Rings | |
| | Major D | Diameter | | Major D | iameter | | Max. N | laterial (| Min. N | laterial |
| Nominal Size | Truncated [Note (1)] | Full Form [Note (2)] | Pitch Diam. [Note (3)] | Truncated [Note (4)] | Full Form [Note (2)] | Pitch Diam. [Note (3)] | Pitch Diam. [Note (3)] | Minor Diam. [Note (5)] | Pitch Diam. [Note (3)] | Minor Diam. [Note (6)] |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 |
| 1/4-20 NC-5 | 0.2380 | 0.2470 | 0.2230 | 0.2362 | 0.2470 | 0.2204 | 0.2175 | 0.1960 | 0.2201 | 0.2060 |
| | 0.2375 | 0.2475 | 0.2229 | 0.2357 | 0.2475 | 0.2205 | 0.2176 | 0.1955 | 0.2200 | 0.2055 |
| 5/16-18 NC-5 | 0.2993 | 0.3090 | 0.2829 | 0.2970 | 0.3090 | 0.2700 | 0.2764 | 0.2520 | 0.2794 | 0.2630 |
| | 0.2988 | 0.3095 | 0.2828 | 0.2965 | 0.3095 | 0.2800 | 0.2765 | 0.2515 | 0.2793 | 0.2625 |
| 3⁄6-16 NC-5 | 0.3605 | 0. 3 710 | 0.3414 | 0.3575 | 0.3710 | 0.3382 | 0.3344 | 0.3070 | 0.3376 | 0.3180 |
| | 0.3599 | 0.3716 | 0.3413 | 0.3569 | 0.3716 | 0.3383 | 0.3345 | 0.3064 | 0.3375 | 0.3174 |
| ⁷ /16-14 NC-5 | 0.4215 | 0.4330 | 0.3991 | 0.4175 | 0.4330 | 0.3955 | 0.3911 | 0.3600 | 0.3947 | 0.3720 |
| | 0.4209 | 0.4336 | 0.3990 | 0.4169 | 0.4336 | 0.3956 | 0.3912 | 0.3594 | 0.3946 | 0.3714 |
| ½-1 3 NC-5 | 0.4828 | 0.4950 | 0.4584 | 0.4783 | 0.4950 | 0.4547 | 0.4500 | 0.4170 | 0.4537 | 0.4290 |
| | 0.4822 | 0.4956 | 0.4582 | 0.4777 | 0.4956 | 0.4548 | 0.4502 | 0.4164 | 0.4536 | 0.4284 |
| ⁹ ⁄16-12 NC-5 | 0.5446 | 0.5575 | 0.5176 | 0.5395 | 0.5575 | 0.5136 | 0.5084 | 0.4720 | 0.5124 | 0.4850 |
| | 0.5440 | 0.5581 | 0.5174 | 0.5389 | 0.5581 | 0.5138 | 0.5086 | 0.4714 | 0.5122 | 0.4844 |
| 5⁄8-11 NC-5 | 0.6058 | 0.6195 | 0.5758 | 0.5998 | 0.6195 | 0.5716 | 0.5660 | 0.5270 | 0.5702 | 0.5400 |
| | 0.6052 | 0.6201 | 0.5756 | 0.5992 | 0.6201 | 0.5718 | 0.5662 | 0.5264 | 0.5700 | 0.5394 |
| 3/4-10 NC-5 | 0.7294 | 0.7440 | 0.6955 | 0.7223 | 0.7440 | 0.6910 | 0.6850 | 0.6420 | 0.6895 | 0.6550 |
| | 0. 7 288 | 0.7446 | 0.6953 | 0.7217 | 0.7446 | 0.6912 | 0.6852 | 0.6414 | 0.6893 | 0.6544 |
| ⁷ / ₈ - 9 NC-5 | 0.8527 | 0.8685 | 0.8144 | 0.8444 | 0.8685 | 0.8095 | 0.8028 | 0.7550 | 0.8077 | 0.7690 |
| | 0.8520 | 0.8692 | 0.8142 | 0.8437 | 0.8692 | 0.8097 | 0.8030 | 0.7543 | 0.8075 | 0.7683 |
| 1 - 8 NC-5 | 0.9764 | 0.9935 | 0.9316 | 0.9664 | 0.9935 | 0.9262 | 0.9188 | 0.8650 | 0.9242 | 0.8800 |
| | 0.9757 | 0.9942 | 0.9314 | 0.9657 | 0.9942 | 0.9264 | 0.9190 | 0.8643 | 0.9240 | 0.8793 |
| 11/8- 7 NC-5 | 1.0 7 64 | 1.1180 | 1.0465 | 1.0871 | 1.1180 | 1.0406 | 1.0322 | 0.9700 | 1.0381 | 0.9860 |
| | 1.0757 | 1.1187 | 1.0463 | 1.0854 | 1.1187 | 1.0408 | 1.0324 | 0.9693 | 1.0379 | 0.9853 |
| 11/4- 7 NC-5 | 1.2242 | 1.2430 | 1.1715 | 1.2121 | 1.2430 | 1.1656 | 1.1572 | 1.0950 | 1.1631 | 1.1110 |
| | 1.2235 | 1.2437 | 1.1713 | 1.2114 | 1.2437 | 1.1658 | 1.1574 | 1.0943 | 1.1629 | 1.1103 |

| | | | W Thread-S | Setting Plugs | | | , AS | | | |
|--|-------------------------|-------------------------|------------------------------|----------------------|-------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| | | Max. Material | | | Min. Material | | O | W Thread-S | etting Rings | |
| | Major D | Diameter | | Major D | jameter | | Max. I | Vlaterial | Min. N | /laterial |
| Nominal Size | Truncated [Note (1)] | Full Form [Note (2)] | Pitch Diam. [Note (3)] | Truncated [Note (4)] | Full Form [Note (2)] | Pitch Diam. (Note (3)] | Pitch Diam. [Note (3)] | Minor Diam. [Note (5)] | Pitch Diam. [Note (3)] | Minor Diam. [Note (6)] |
| 1 | 2 | 3 | 4 | 5 | 6 1 | 7 | 8 | 9 | 10 | 11 |
| 1 ³ / ₈ - 6 NC-5 | 1.3470 1.3462 | 1.3680 1.3688 | 1.2839 1.2837 | 1.3319 1.3311 | 1.3680 1.3688 | 1.2768 1.2770 | 1.2667 1.2669 | 1.1950 1.1942 | 1.2738 1.2736 | 1.2130 1.2122 |
| 1½- 6 NC-5 | 1.4720 1.4712 | 1.4930 1.4938 | 1.4089 1.4087 | 1.4569 1.4561 | 1.4930 1.4938 | 1.4018 1.4020 | 1.3917 1.3919 | 1.3200 1.3192 | 1.3988 1.3986 | 1.3380 1.3372 |

NOTES:

- (1) Maximum-material truncated major diameter equals maximum major diameter of external thread series NC-5 CSF minus $(0.06\sqrt[3]{p^2} + 0.017p)$, W tolerance minus.
- (2) Full-form major diameter equals maximum major diameter of external thread series NC-5 CSF, W tolerance plus.
- (3) Pitch diameter tolerances greater than W are acceptable for setting indicating gages only when the indicating gage is set to the calibrated pitch diameter.
- (4) Minimum-material truncated major diameter equals maximum major diameter of external thread series NC-5 CSF minus 0.25H, W tolerance minus.
- (5) Maximum-material minor diameter equals minimum minor diameter of internal thread series NC-5 INF, W tolerance minus.
- (6) Minimum-material minor diameter equals maximum minor diameter of internal thread series NC-5 INF, W tolerance minus.

APPENDIX A

Obsolete Tentative Standard and Alternate Standard for Class 5 Interference-Fit Thread (Not to Be Used for New Design)

(This Appendix is not part of ASME/ANSI B1.12-1987, and is included for information purposes only.)

A1 INTRODUCTION

Appendix A contains useful information that is supplementary to this Standard.

Since Class 5 interference-fit threads based on both the obsolete Tentative Standard and the obsolete Alternate Standard are still in use today on spare parts in stock and appear on many drawings, the following profiles and tables on limits of size and gages are reproduced. The data is for hardened steel studs set in hard materials, i.e., cast iron, steel, and bronze.

NOTE: In comparison to the Tentative Standard, the Alternate Standard provided increased tolerances on hole threads and reduced tolerances on stud threads. Therefore, studs produced to the Tentative Standard must be installed only in holes produced to the Tentative Standard and those produced to the Alternate Standard installed only in holes produced to the Alternate Standard.

Percentages of interference metal per turn of engagement, compared to NC-5 HF/IF at 100%, are given in Table D1 for the Tentative and Alternate Standards.

A2 TENTATIVE STANDARD

Tentative American National Standard Class 5 Interference Fit Threads was published by the National Screw Thread Commission in 1928 and 1933 and by the National Bureau of Standards in Handbooks H25-1939, H28-1942, and H28-1950.

A2.1 Size Limits and Thread Profiles

Tables A1, A2, A3, and A4 give the tolerances, allowances, and limits of size for both coarse and fine thread series. Figures A1, A2, and A3 show thread profiles.

A2.2 Acceptability

Product thread acceptability shall be in accordance with ANSI/ASME B1.3M based upon the method specified. Gages shall be designed in accordance with the principles in ANSI/ASME B1.2.

A3 ALTERNATE STANDARD

The Alternate Standard, American National Class 5 Interference Fit Threads, was published by the National Bureau of Standards in Handbooks H28-1942 and H28-1944.

A3.1 Size Limits and Thread Profiles

Tables A5, A6, A7, and A8 give the tolerances, allowances, and limits of size for both coarse and fine thread series. Figures A1, A4, and A5 show thread profiles.

A3.2 Acceptability

Product thread acceptability shall be in accordance with ANSI/ASME B1.3M based upon the method specified. Gages are in accordance with ANSI/ASME B1.2, except Tables A9, A10, A11, and A12 give the limits of size for all gages.

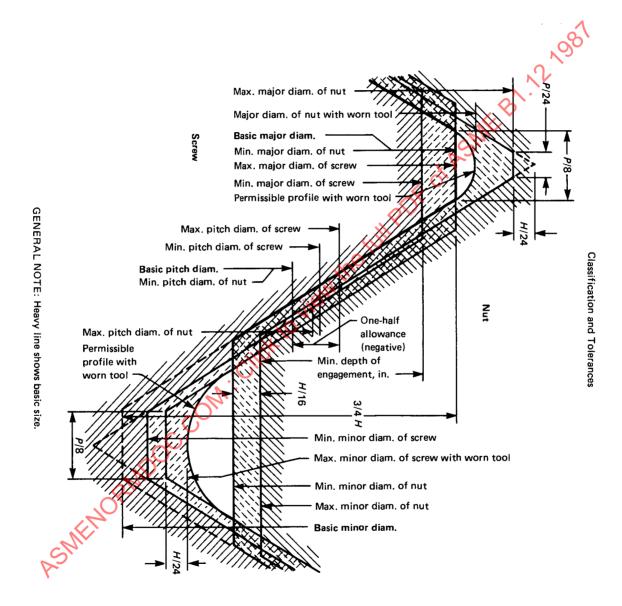
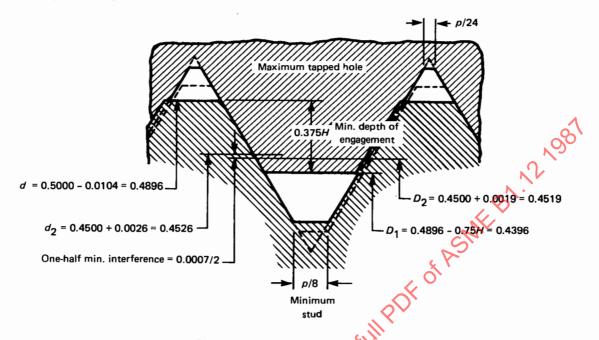


ILLUSTRATION OF TOLERANCES, ALLOWANCES, AND CREST CLEARANCES FOR TENTATIVE AND ALTERNATE CLASS 5 FIT FOR THREADED STUDS



GENERAL NOTE: Broken line shows basic size.

FIG. A2 ILLUSTRATION OF LOOSEST CONDITION FOR TENTATIVE CLASS 5 WRENCH FIT FOR THREADED STUDS, ½ in., 13 THREADS, SET IN HARD MATERIALS

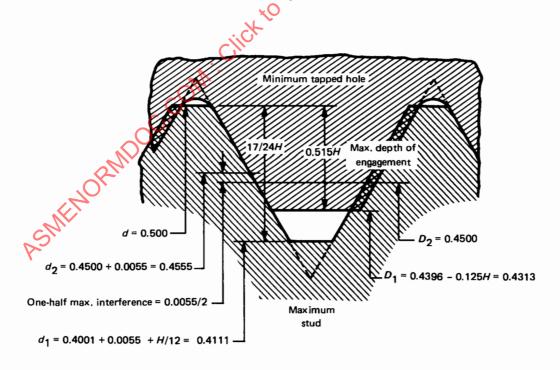


FIG. A3 ILLUSTRATION OF TIGHTEST CONDITION FOR TENTATIVE CLASS 5 WRENCH FIT FOR THREADED STUDS, ½ in., 13 THREADS, SET IN HARD MATERIALS

TABLE A1 TENTATIVE CLASS 5 WRENCH FIT FOR THREADED STUDS, ALLOWANCES AND TOLERANCES FOR STUDS AND TAPPED HOLES, COARSE THREADED STUDS SET IN HARD MATERIALS

| - | | | rence on imeter, in. | | iameter ces, in. | 1 | Tolera | | alf of |
|---|---------------------|---------|-------------------------|------------|---------------------|---|--------|---|--------------|
| Nominal Size 1 1/4 5/16 3/8 7/16 1/2 9/16 5/8 | Threads per inch | Minimum | Maximum | Stud | Tapped Hole | s | tud | | pped lole |
| | 2 | 3 | 4 | √ 5 | 6 | 7 | | 8 | |
| 1/4 | 20 | 0.0003 | 0.0018 | 0.0007 | 0.0008 | 0 | 16 | 0 | 25 |
| 5/16 | 18 | 0.0005 | 0.0040 | 0.0020 | 0.0015 | 0 | 41 | 0 | 31 |
| 3/8 | 16 | 0.0005 | 0.0045 | 0.0024 | 0.0016 | 0 | 44 | 0 | 29 |
| 7/16 | 14 | 0.0006 | 0.0050 | 0.0026 | 0.0018 | 0 | 42 | 0 | 29 |
| 1/2 | 13 | 0.0007 | 0.0055 | 0.0029 | 0.0019 | 0 | 44 | 0 | 28 |
| 9/16 | 12 | 0.0008 | 0.0060 | 0.0032 | 0.0020 | 0 | 44 | 0 | 28 |
| 5/8 | 11 | 0.0008 | 0.0060 | 0.0031 | 0.0021 | 0 | 39 | 0 | 26 |
| 3/4 | 10 | 0.0009 | 0.0065 | 0.0033 | 0.0023 | 0 | 38 | 0 | 26 |
| 7/8 | 9 | 0.0010 | 0.0065 | 0.0031 | 0.0024 | 0 | 32 | 0 | 25 |
| 1 | | 0.0011 | 0.0065 | 0.0027 | 0.0027 | 0 | 25 | 0 | 25 |
| · 1 1/8 | 8 7 | 0.0011 | 0.0065 | 0.0024 | 0.0030 | 0 | 19 | 0 | 24 |
| 11/4 | 7 | 0.0012 | 0.0065 | 0.0023 | 0.0030 | 0 | 18 | 0 | 24 |
| 13/8 | 6 | 0.0012 | 0.0065 | 0.0017 | 0.0036 | 0 | 12 | 0 | 25 |
| 11/2 | 261 | 0.0013 | 0.0070 | 0.0021 | 0.0036 | 0 | 14 | 0 | 25 |

TABLE A2 TENTATIVE CLASS 5 WRENCH FIT FOR THREADED STUDS, ALLOWANCES AND TOLERANCES FOR STUDS AND TAPPED HOLES, FINE THREADED STUDS SET IN HARD MATERIALS

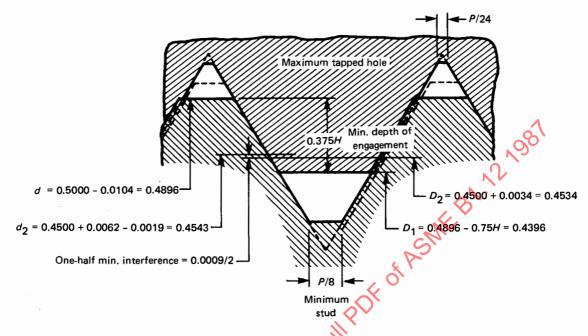
| | | | rence on imeter, in. | | iameter ices, ip: | | Toler | | alf of |
|-----------------|---------------------|---------|-------------------------|---------|----------------------|---|-------|----|--------------|
| Nominal Size | Threads per inch | Minimum | Maximum | Stud | Tapped Hole | S | Stud | 1 | pped lole |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | | 8 | |
| 1/4 | 28 | 0.0005 | 0.0034 | 0.0018 | 0.0011 | 0 | 58 | 0 | 35 |
| 5/16 | 24 | 0.0005 | 0.0037 | 0.0020 | 0.0012 | 0 | 55 | 0 | 33 |
| 3/8 | 24 | 0.0006 | 0.0044 | 10.0026 | 0.0012 | 1 | 11 | 0 | 33 |
| 7/16 | 20 | 0.0006 | 0.0044 | 0.0025 | 0.0013 | 0 | 57 | 0 | 30 |
| 1/2 | 20 | 0.0007 | 0.0050 | 0.0030 | 0.0013 | 1 | 9 | 0 | 30 |
| 9/16 | 18 | 0.0007 | 0.0050 | 0.0028 | 0.0015 | 0 | 58 | o | 31 |
| 5/8 | 18 | 0.0008 | 0.0055 | 0.0032 | 0.0015 | 1 | 6 | 0 | 31 |
| 3/4 | 16 | 0.0008 | 0.0059 | 0.0035 | 0.0016 | 1 | 4 | 0 | 29 |
| 7/8 | 14 | 0.0008 | 0.0061 | 0.0035 | 0.0018 | 0 | 56 | О | 29 |
| 1 | 14 | 0.0009 | 0.0069 | 0.0042 | 0.0018 | 1 | 7 | lo | 29 |
| 11/8 | 12 | 0.0009 | 0.0067 | 0.0038 | 0.0020 | 0 | 52 | ا | 28 |
| 1 1/4 | 12 | 0.0011 | 0.0060 | 0.0029 | 0.0020 | 0 | 40 | 0 | 28 |
| 1 3/8 | 12 | 0.0011 | 0.0055 | 0.0024 | 0.0020 | 0 | 33 | 0 | 28 |
| 1 1/2 | 12 | 0.0012 | 0.0050 | 0.0018 | 0.0020 | 0 | 25 | Ιo | 28 |

TABLE A3 LIMITING DIMENSIONS FOR TENTATIVE CLASS 5 WRENCH FIT FOR AMERICAN NATIONAL COARSE THREAD SERIES, STEEL STUDS SET IN HARD MATERIALS (CAST IRON, SEMISTEEL, BRONZE, ETC.)

| | | | | Stud Sizes | 1 | | | Tap | ped Hole S | lizes | | | | | |
|-----------------|------------------|-----------------|----------------|------------|----------------|------------------------|---------|----------------|------------|----------------|------------------------|--|---------------|--|--------------------|
| | | | iameter, n. | _ | iameter, 1. | Minor Diam., in. | Minor D | iameter, 1. | | iameter, n. | Major Diam., in. | Recomme Drill | • | Approx Torque Engager 1½ <i>D</i> , | at Full nent of |
| Nominal Size | Threads per inch | Max. | Min. | Max. | Min. | Max. | Min. | Max. | Ø Min. | Max. | Min. | Nominal Size | Diam., in. | Max. | Min. |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | (C9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
| 1/4 | 20 | 0.2500 | 0.2428 | 0.2193 | 0.2186 | 0.1904 | 0.2049 | 0.2103 | 0.2175 | 0.2183 | 0.2500 | No. 4 | 0.2090 | 105 | 35 |
| 5/16 | 18 | 0.3125 | 0.3043 | 0.2804 | 0.2784 | 0.2483 | 0.2622 | 0.2682 | 0.2764 | 0.2779 | 0.3125 | н | 0.2660 | 265 | 80 |
| 3/8 | 16 | 0.3750 | 0.3660 | 0.3389 | 0.3365 | 0.3028 | 0.3186 | 0.3254 | 0.3344 | 0.3360 | 0.3750 | P | 0.3230 | 420 | 120 |
| 7/16 | 14 | 0.43 7 5 | 0.4277 | 0.3961 | 0.3935 | 0.3549 | 0.3736 | 0.3813 | 0.3911 | 0.3929 | 0.4375 | V | 0.3770 | 610 | 180 |
| 1/2 | 13 | 0.5000 | 0.4896 | 0.4555 | 0.4526 | 0.4111 | 0.4313 | 0.4396 | 0.4500 | 0.4519 | 0.5000 | 7/16 | 0.4375 | 850 | 265 |
| 9/16 | 12 | 0.5625 | 0.5513 | 0.5144 | 0.5112 | 0.4663 | 0.4882 | 0.4972 | 0.5084 | 0.5104 | 0.5625 | 12.5 mm | 0.4921 | 1,170 | 360 |
| 5/8 | 11 | 0.6250 | 0.6132 | 0.5720 | 0.5689 | 0.5195 | 0.5444 | 0.5542 | 0.5660 | 0.5681 | 0.6250 | 35/64 | 0.5469 | 1,450 | 450 |
| 3/4 | 10 | 0.7500 | 0.7372 | 0.6915 | 0.6882 | 0.6338 | 0.6614 | 0.6722 | 0.6850 | 0.6873 | 0.7500 | 43/64 | 0.6719 | 2,300 | 730 |
| 7/8 | 9 | 0.8750 | 0.8610 | 0.8093 | 0.8062 | 0.7452 | 0.7768 | 0.7888 | 0.8028 | 0.8052 | 0.8750 | 25/32 | 0.7812 | 3,200 | 1,080 |
| 1 | 8 | 1.0000 | 0.9848 | 0.9253 | 0.9226 | 0.8531 | 0.8901 | 0.9036 | 0.9188 | 0.9215 | 1.0000 | ⁵⁷ / ₆₄ | 0.8906 | 4,250 | 1,500 |
| 1 1/8 | 7 | 1.1250 | 1.1080 | 1.0387 | 1.0363 | 0.9562 | 0.9998 | 1.0152 | 1.0322 | 1.0352 | 1.1250 | 1 | 1.0000 | 5,300 | 1,875 |
| 1 1/4 | 7 | 1.2500 | 1.2330 | 1,1637 | 1.1614 | 1.0812 | 1.1248 | 1.1402 | 1.1572 | 1.1602 | 1.2500 | 1 ½ | 1.1250 | 6,950 | 2,535 |
| 13/8 | 6 | 1.3750 | 1.3548 | 1,2732 | 1.2715 | 1.1770 | 1.2286 | 1.2466 | 1.2667 | 1.2703 | 1.3750 | 1 15/64 | 1.2344 | 8,150 | 2,970 |
| 1 1/2 | 6 | 1.5000 | 1.4798 | 1.3987 | 1.3966 | 1.3025 | 1.3536 | 1.3716 | 1.3917 | 1.3953 | 1.5000 | 1 ²³ / ₆₄ | 1.3594 | 10,400 | 3,900 |

TABLE A4 LIMITING DIMENSIONS FOR TENTATIVE CLASS 5 WRENCH FIT FOR AMERICAN NATIONAL FINE THREAD SERIES, STEEL STUDS SET IN HARD MATERIALS (CAST IRON, SEMISTEEL, BRONZE, ETC.)

| | | | | Stud Sizes | } | | | Тар | ped Hole S | izes | CMIL | | | Approx | rimate |
|------------------|------------------|--------|----------------|------------|----------------|------------------------|--------|----------------|------------|---------|------------------------|------------------|---------------|----------------------------|--------------------|
| | | _ | iameter, n. | 1 | iameter, n. | Minor Diam., in. | | iameter, 1. | 1 | iameter | Major Diam., in. | Recomme Drill | • | Torque Engager 1½ D, | at Full nent of |
| Nominal Size | Threads per inch | Max. | Min. | Max. | Min. | Max. | Min. | Max. | Mig | Max. | Min. | Nominal Size | Diam., in. | Max. | Min. |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
| 1/4 | 28 | 0.2500 | 0.2438 | 0.2302 | 0.2284 | 0.2096 | 0.2167 | 0.2206 | 0.2268 | 0.2279 | 0.2500 | 7/32 | 0.2188 | 140 | 45 |
| 5/16 | 24 | 0.3125 | 0.3059 | 0.2891 | 0.2871 | 0.2650 | 0.2743 | 0.2788 | 0.2854 | 0.2866 | 0.3125 | J | 0.2770 | 230 | 70 |
| 3/8 | 24 | 0.3750 | 0.3684 | 0.3523 | 0.3497 | 0.3282 | 0.3368 | 0.3413 | 0.3479 | 0.3491 | 0.3750 | R | 0.3390 | 410 | 125 |
| ⁷ /16 | 20 | 0.4375 | 0.4303 | 0.4094 | 0.4069 | 0.3805 | 0.3924 | 0.3978 | 0.4050 | 0.4063 | 0.4375 | × | 0.3970 | 540 | 170 |
| 1/2 | 20 | 0.5000 | 0.4928 | 0.4725 | 0.4695 | 0.4436 | 0.4549 | 0.4603 | 0.4675 | 0.4688 | 0.5000 | | 0.4576 | 810 | 260 |
| 9/ ₁₆ | 18 | 0.5625 | 0.5543 | 0.5314 | 0.5286 | 0.4993 | 0.5122 | 0.5182 | 0.5264 | 0.5279 | 0.5625 | 33/64 | 0.5156 | 1.040 | 330 |
| 5/8 | 18 | 0.6250 | 0.6168 | 0.5944 | 0.5912 | 0.5623 | 0.5747 | 0.5807 | 0.5889 | 0.5904 | 0.6250 | 37/64 | 0.5781 | 1,430 | 460 |
| 3/4 | 16 | 0.7500 | 0.7410 | 0.7153 | 0.7118 | 0.6792 | 0.6936 | 0.7004 | 0.7094 | 0.7110 | 0.7500 | | 0.6970 | 2,200 | 685 |
| | | | | | | . 1 | | 1 | | | | | ĺ | | |
| ⁷ /8 | 14 | 0.8750 | 0.8652 | 0.8347 | 0.8312 | 0.7935 | 0.8111 | 0.8188 | 0.8286 | 0.8304 | 0.8750 | 13/16 | 0.8125 | 3,070 | 945 |
| 1 | 14 | 1.0000 | 0.9902 | 0.9605 | 0.9563 | 0.9193 | 0.9361 | 0.9438 | 0.9536 | 0.9554 | 1.0000 | 15/16 | 0.9375 | 4,590 | 1,410 |
| 1 1/8 | 12 | 1.1250 | 1.1138 | 1.0776 | 1.0738 | 1.0295 | 1.0507 | 1.0597 | 1.0709 | 1.0729 | 1.1250 | | 1.0552 | 5,620 | 1,750 |
| 11/4 | 12 | 1.2500 | 1.2388 | 1.2019 | 1,1990 | 1.1538 | 1.1757 | 1.1847 | 1.1959 | 1.1979 | 1.2500 | 30.0 mm | 1.1811 | 6,960 | 2,530 |
| 1 3/8 | 12 | 1.3750 | 1.3638 | 1.3264 | 1 3240 | 1.2782 | 1.3007 | 1.3097 | 1.3209 | 1.3229 | 1.3750 | | 1.3052 | 8,440 | 3,225 |
| 1 1/2 | 12 | 1.5000 | 1.4888 | 1.4509 | 1.4491 | 1.4028 | 1.4257 | 1.4347 | 1.4459 | 1.4479 | 1.5000 | | 1.4302 | 10,070 | 4,215 |



GENERAL NOTE: Broken line shows basic size.

FIG. A4 ILLUSTRATION OF LOOSEST CONDITION FOR ALTERNATE CLASS 5 FIT FOR THREADED STUDS, ½ in., 13 THREADS, SET IN HARD MATERIALS

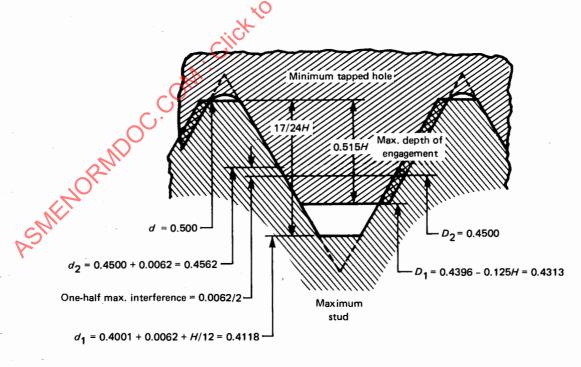


FIG. A5 ILLUSTRATION OF TIGHTEST CONDITION FOR ALTERNATE CLASS 5 FIT FOR THREADED STUDS, $\frac{1}{2}$ in., 13 THREADS, SET IN HARD MATERIALS

TABLE A5 ALTERNATE CLASS 5 FIT FOR THREADED STUDS, ALLOWANCES AND TOLERANCES FOR STUDS AND TAPPED HOLES, COARSE THREADED STUDS SET IN HARD MATERIALS

| | | Interference on F | Pitch Diameter, in. | Pitch Diameter | Tolerances, in. |
|-------------------|---------------------|-------------------|---------------------|----------------|-----------------|
| Nominal Size | Threads per inch | Minimum | Maximum | Stud | Tapped Hole |
| 1 | 2 | 3 | 4 | 5 | √95 6 |
| 5/16 | 18 | 0.0005 | 0.0046 | 0.0015 | 0.0026 |
| 3/8 | 16 | 0.0005 | 0.0051 | 0.0016 | 0.0030 |
| ⁷ /16 | 14 | 0.0007 | 0.0057 | 0.0018 | 0.0032 |
| 1/2 | 13 | 0.0009 | 0.0062 | 0.0019 | 0.0034 |
| 9/16 | 12 | 0.0011 | 0.0066 | 0.0020 | 0.0035 |
| 5/8 | 11 | 0.0012 | 0.0069 | 0.0021 | 0.0036 |
| 3/4 | 10 | 0.0013 | 0.0073 | 0.0023 | 0.0037 |
| 7/8 | 9 | 0.0013 | 0.0074 | 0.0024 | 0.0037 |
| 1 | 8 | 0.0013 | 0.0075 | 0.0025 | 0.0037 |
| 1 1/a | 7 | 0.0014 | 0.0076 | 0.0025 | 0.0037 |
| 11/4 | 7 | 0.0014 | 0.0076 | 0.0025 | 0.0037 |
| 1 3/ ₈ | 6 | 0.0014 | 0.0076 | 0.0025 | 0.0037 |
| 1 1/2 | 6 | 0.0016 | 0.0081 | 0.0025 | 0.0040 |

TABLE A6 ALTERNATE CLASS 5 FIT FOR THREADED STUDS, ALLOWANCES AND TOLERANCES FOR STUDS AND TAPPED HOLES, FINE THREADED STUDS SET IN HARD MATERIALS

| | - | Interference on F | Pitch Diameter, in. | Pitch Diameter Tolerances, in. | | | | |
|-------------------------------|------------------|-------------------|---------------------|--------------------------------|----------------|--|--|--|
| Nominal Size | Threads per inch | Minimum | Maximum | Stud | Tapped Hole | | | |
| 1 | 22 | 3 | 4 | 5 | 6 | | | |
| 1/4 | 28 | 0.0006 | 0.0039 | 0.0011 | 0.0022 | | | |
| . 5/16 | 24 | 0.0006 | 0.0042 | 0.0012 | 0.0024 | | | |
| 3/8 | 24 | 0.0008 | 0.0044 | 0.0012 | 0.0024 | | | |
| 7/16 | 20 | 0.0008 | 0.0047 | 0.0013 | 0.0026 | | | |
| 1/2 | 20 | 0.0011 | 0.0050 | 0.0013 | 0.0026 | | | |
| 9/16 | 18 | 0.0011 | 0.0056 | 0.0015 | 0.0030 | | | |
| 5/8 | 18 | 0.0011 | 0.0056 | 0.0015 | 0.0030 | | | |
| 3/4 | 16 | 0.0011 | 0.0059 | 0.0016 | 0.0032 | | | |
| ⁷ /8 | 14 | 0.0011 | 0.0065 | 0.0018 | 0.0036 | | | |
| 1 | 14 | 0.0015 | 0.0069 | 0.0018 | 0.0036 | | | |
| 1 ½ | 12 | 0.0015 | 0.0075 | 0.0020 | 0.0040 | | | |
| 1 1/4 | 12 | 0.0015 | 0.0072 | 0.0020 | 0.0037 | | | |
| 1 ³ / ₈ | 12 | 0.0015 | 0.0067 | 0.0020 | 0.0032 | | | |
| 1 1/2 | 12 | 0.0015 | 0.0062 | 0.0020 | 0.0027 | | | |

TABLE A7 LIMITING DIMENSIONS FOR ALTERNATE CLASS 5 FIT, AMERICAN NATIONAL COARSE THREAD SERIES, STEEL STUDS SET IN HARD MATERIALS (CAST IRON, SEMISTEEL, BRONZE, ETC.)

| | | | | Stud Sizes | | | | Тар | ped Hole S | izes | | | | Approx | imata |
|-----------------|------------------|---------|----------------|----------------|--------|------------------------|---------|--------|------------|--------|------------------------|-------------------------------|--------|------------------------------------|--------------------|
| | | Major D | iameter, n. | Pitch Di ir | | Minor Diam., in. | Minor D | | Pitch Di | | Major Diam., in. | Recomme Drill Siz | • | Torque Engagen 1½ <i>D</i> , | at Full nent of |
| Nominal Size | Threads per inch | Max. | Min. | Max. | Min. | Max. | Min. | Max. | Min. | Max. | Min. | Nominal Size | Diam. | Max. | Min. |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | iles | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
| 5/16 | 18 | 0.3125 | 0.3043 | 0.2810 | 0.2795 | 0.2489 | 0.2622 | 0.2682 | 0.2764 | 0.2790 | 0.3125 | 0.2656 | 0.2656 | 265 | 80 |
| 3/ _B | 16 | 0.3750 | 0.3660 | 0.3395 | 0.3379 | 0.3034 | 0,3186 | 0.3254 | 0.3344 | 0.3374 | 0.3750 | 0.3230 | 0.3230 | 420 | 120 |
| 7/16 | 14 | 0.4375 | 0.4277 | 0.3968 | 0.3950 | 0.3556 | 0.3736 | 0.3813 | 0.3911 | 0.3943 | 0.4375 | 0.3750 | 0.3750 | 610 | 195 |
| 1/2 | 13 | 0.5000 | 0.4896 | 0.4562 | 0.4543 | 0.4118 | 0.4313 | 0.4396 | 0.4500 | 0.4534 | 0.5000 | 0.4375 | 0.4375 | 850 | 295 |
| 9/16 | 12 | 0.5625 | 0.5513 | 0.5150 | 0.5130 | 0.4669 | 0.4882 | 0.4972 | 0.5084 | 0.5119 | 0.5625 | 12.5 mm | 0.4921 | 1,170 | 425 |
| 5/8 | 11 | 0.6250 | 0.6132 | 0.5729 | 0.5708 | 0.5204 | 0.5444 | 0.5542 | 0.5660 | 0.5696 | 0.6250 | ³⁵ / ₆₄ | 0.5469 | 1,450 | 560 |
| 3/4 | 10 | 0.7500 | 0.7372 | 0.6923 | 0.6900 | 0.6346 | 0.6614 | 0.6722 | 0.6850 | 0.6887 | 0.7500 | ⁴³ / ₆₄ | 0.6719 | 2,300 | 880 |
| 7/8 | 9 | 0.8750 | 0.8610 | 0.8102 | 0.8078 | 0.7461 | 0.7768 | 0.7888 | 0.8028 | 0.8065 | 0.8750 | ²⁵ /32 | 0.7812 | 3,200 | 1,230 |
| 1 | 8 | 1.0000 | 0.9848 | 0.9263 | 0.9238 | 0.8541 | 0.8901 | 0.9036 | 0.9188 | 0.9225 | 1.0000 | 57/64 | 0.8906 | 4,250 | 1,630 |
| 1 ½ | 7 | 1.1250 | 1.1080 | 1.0398 | 1.0373 | 0.9573 | 0.9998 | 1.0152 | 1.0322 | 1.0359 | 1.1250 | 1 | 1.0000 | 5,300 | 2,120 |
| 11/4 | 7 | 1.2500 | 1.2330 | 1.1648 | 1.1623 | 1.0823 | 1.1248 | 1.1402 | 1.1572 | 1.1609 | 1.2500 | 1 ½ | 1.1250 | 6,950 | 2,780 |
| 13/8 | 6 | 1.3750 | 1.3548 | 1 2743 | 1.2718 | 1.1781 | 1.2286 | 1.2466 | 1.2667 | 1.2704 | 1.3750 | 115/64 | 1.2344 | 8,150 | 3,210 |
| 1 1/2 | 6 | 1.5000 | 1.4796 | 1.3998 | 1.3973 | 1.3036 | 1.3536 | 1.3716 | 1.3917 | 1.3957 | 1.5000 | 1 23/64 | 1.3594 | 10,400 | 4,340 |

TABLE A8 LIMITING DIMENSIONS FOR ALTERNATE CLASS 5 FIT, AMERICAN NATIONAL FINE THREAD SERIES, STEEL STUDS SET IN HARD MATERIALS (CAST IRON, SEMISTEEL, BRONZE, ETC.)

| | | | | Stud Sizes | : | | | Тар | ped Hole S | izes | | | Approx | imate | |
|--------------------|------------------|--------|-----------------------|------------|------------------------|--------|------------------------|--------|--------------------|--------|------------------------|------------------------------------|--------|---|-------|
| | | | ajor Diameter, in. | | Pitch Diameter, in. | | Minor Diameter, in. | | Pitch Diameter in. | | Major Diam., in. | Recommended Tap Drill Size, in. | | Torque at Full Engagement of 11/2 D, lb-in. | |
| Nominal Size | Threads per inch | Max. | Min. | Max. | Min. | Max. | Min. | Max. | Min. | Max. | Min. | Nominal Size | Diam. | Max. | Min. |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 70 | 11 | 12 | 13 | 14 | 15 | 16 |
| 1/4 | 28 | 0.2500 | 0.2436 | 0.2307 | 0.2296 | 0.2101 | 0.2167 | 0.2206 | 0.2268 | 0.2290 | 0.2500 | 0.2187 | 0.2187 | 140 | 50 |
| 5/16 | 24 | 0.3125 | 0.3059 | 0.2896 | 0.2884 | 0.2655 | 0.2743 | 0.2788 | 0.2854 | 0.2878 | 0.3125 | 0.2770 | 0.2770 | 230 | 80 |
| 3/8 | 24 | 0.3750 | 0.3684 | 0.3523 | 0.3511 | 0.3282 | 0.3368 | 03413 | 0.3479 | 0.3503 | 0.3750 | 0.3390 | 0.3390 | 410 | 145 |
| ⁷ /16 . | 20 | 0.4375 | 0.4303 | 0.4097 | 0.4084 | 0.3808 | 0.3924 | 0.3978 | 0.4050 | 0.4076 | 0.4375 | 0.3970 | 0.3970 | 540 | 195 |
| 1/2 | 20 | 0.5000 | 0.4928 | 0.4725 | 0.4712 | 0.4436 | 0.4549 | 0.4603 | 0.4675 | 0.4701 | 0.5000 | | 0.4576 | 810 | 320 |
| 9/16 | 18 | 0.5625 | 0.5543 | 0.5320 | 0.5305 | 0.4999 | 0.5122 | 0.5182 | 0.5264 | 0.5294 | 0.5625 | 33/64 | 0.5156 | 1,040 | 410 |
| 5/B | 18 | 0.6250 | 0.6168 | 0.5945 | 0.5930 | 0.5624 | 0.5747 | 0.5807 | 0.5889 | 0.5919 | 0.6250 | 37/64 | 0.5781 | 1,430 | 540 |
| 3/4 | 16 | 0.7500 | 0.7410 | 0.7153 | 0.7137 | 0.6792 | 0.6936 | 0.7004 | 0.7094 | 0.7126 | 0.7500 | | 0.6970 | 2,200 | 805 |
| 7/ _B | 14 | 0.8750 | 0.8652 | 0.8351 | 0.8333 | 0.7939 | 0.8111 | 0.8188 | 0.8286 | 0.8322 | 0.8750 | 13/16 | 0.8125 | 3,070 | 1,110 |
| 1 | 14 | 1.0000 | 0.9902 | 0.9605 | 0.9587 | 0.9193 | 0.9361 | 0.9438 | 0.9536 | 0.9572 | 1.0000 | 15/16 | 0.9375 | 4,590 | 1,820 |
| 11/8 | 12 | 1.1250 | 1.1138 | 1.0784 | 1.0764 | 1.0303 | 1.0507 | 1.0597 | 1.0709 | 1.0749 | 1.1250 | | 1.0552 | 5,620 | 2,260 |
| 1 1/4 | 12 | 1.2500 | 1.2388 | 1.2031 | 1.201 | 1.1550 | 1.1757 | 1.1847 | 1.1959 | 1.1996 | 1.2500 | 30.0 mm | 1.1811 | 6,960 | 2,960 |
| 13/8 | 12 | 1.3750 | 1.3638 | 1.3276 | 1.3256 | 1.2795 | 1.3007 | 1.3097 | 1.3209 | 1.3241 | 1.3750 | | 1.3052 | 8,440 | 3,770 |
| 11/2 | 12 | 1.5000 | 1.4888 | 1.4521 | 1.4501 | 1.4040 | 1.4257 | 1.4347 | 1.4459 | 1.4486 | 1.5000 | | 1.4302 | 10,070 | 4,710 |

TABLE A9 LIMITING DIMENSIONS OF SETTING PLUG AND THREAD WORKING GAGES AND PLAIN DIAMETER GAGES FOR ALTERNATE CLASS 5 FIT THREADED STUDS, AMERICAN NATIONAL COARSE THREAD SERIES

| | | ı | | | | | | Size, in. | ≫. | | | | | | |
|---|--------------|------------------|------------------|-------------------|-------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|-------------------|---------|--|
| | | 5/16 | 3/8 | 7/16 | 1/2 | 9/16 | 5/ _B | 3/40 | ⁷ /8 | 1 | 1 ½ | 11/4 | 1 ³ /8 | 11/2 | |
| | | Threads per inch | | | | | | | | | | | | | |
| Limiting Dimensions | | 18 | 16 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 7 | 6 | 6 | |
| GO Thread Gages for Studs | | | | | | | KILL. | | | | | | | | |
| Major diameter of full-form setting plug and full portion of | Max. | 0.3176 | 0.3807 | 0.4438 | 0.5068 | 0.5697 | 0.6325 | 0.7579 | 0.8831 | 1.0082 | 1.1333 | 1.2583 | 1.3834 | 1.5089 | |
| truncated setting plug | Min. | 0.3171 | 0.3801 | 0.4432 | 0.5062 | 0.5691 | 0.6319 | 0.7573 | 0.8824 | 1.0075 | 1.1326 | 1.2576 | 1.3826 | 1.5081 | |
| Major diameter of truncated portion of truncated setting plug | Max. | 0.3043 | 0.3660 | 0.4277 | 0.4896 | 0.5513 | 0.6132 | 0.7372 | 0.8610 | 0.9846 | 1.1080 | 1.2330 | 1.3548 | 1.4798 | |
| | Min. | 0.3038 | 0.3654 | 0.4271 | 0.4890 | 0.5507 | 0.6126 | 0.7366 | 0.8603 | 0.9841 | 1.1073 | 1.2323 | 1.3540 | 1.4790 | |
| Pitch diameter of setting plug and working gages | Max. | 0.2810 | 0.3395 | 0.3968 | 0.4562 | 0.5150 | 0.5729 | 0.6923 | 0.8102 | 0.9263 | 1.0398 | 1.1648 | 1.2743 | 1.3998 | |
| | Min. | 0.2809 | 0.3394 | 0.39665 | 0.45605 | 0.5148 | 0.5727 | 0.6921 | 0.8100 | 0.9261 | 1.0396 | 1.1646 | 1.2741 | 1.3996 | |
| Minor diameter of gages | Max. | 0.2570 | 0.3124 | 0.3659 | 0.4229 | 0.4789 | 0.5335 | 0.6490 | 0.7621 | 0.8722 | 0.9780 | 1.1030 | 1.2022 | 1.3277 | |
| | Min. | 0.2565 | 0.3118 | 0.3653 | 0.4223 | 0.4783 | 0.5329 | 0.6484 | 0.7614 | 0.8715 | 0.9773 | 1.1623 | 1.2014 | 1.3269 | |
| NOT GO Thread Gages for Studs | | | 1 | ٠ | | | | | | | | | | | |
| Major diameter of full-form setting plug and full portion of truncated setting plug | Min. | 0.3171 | 0,3801 | 0.4432 | 0.5062 | 0.5691 | 0.6319 | 0.7573 | 0.8824 | 1.0075 | 1.1326 | 1.2576 | 1.3826 | 1.5081 | |
| | Max. | 0.3176 | 0.3807 | 0.4438 | 0.5068 | 0.5697 | 0.6325 | 0.7579 | 0.8831 | 1.0082 | 1.1333 | 1.2583 | 1.3834 | 1.5089 | |
| Major diameter of truncated portion of truncated setting plug | Min. | 0.3031 | 0.3644 | 0.4253 | 0.4870 | 0.5485 | 0.6096 | 0.7327 | 0.8552 | 0.9772 | 1.0985 | 1.2235 | 1.3432 | 1.4687 | |
| | Max. | 0.3036 | 0.3650 | 0.4259 | 0.4876 | 0.5491 | 0.6102 | 0.7333 | 0.8559 | 0.9779 | 1.0992 | 1.2242 | 1.3440 | 1.4695 | |
| Pitch diameter of setting plug and working gages for production and inspection | Min. Max. | 0.2795 0,2796 | 0.3379 0.3380 | 0.3950 0.39515 | 0.4543 0.45445 | 0.5130 0.5132 | 0.5708 0.5710 | 0.6900 0.6902 | 0.8078 0.8080 | 0.9238 0.9240 | 1.0373 1.0375 | 1.1623 1.1625 | 1.2718 1.2720 | 1.3973 | |
| Plain Diameter Gage for Studs | <i>O</i> , | | | | | | | | | | | | | | |
| GO gage for major diameter | Max. | 0.31250 | 0.37500 | 0.43750 | 0.50000 | 0.56250 | 0.62500 | 0.75000 | 0.87500 | 1.00000 | 1.12500 | 1.25000 | 1.37500 | 1.50000 | |
| | Min. | 0.31243 | 0.37493 | 0.43743 | 0.49993 | 0.56243 | 0.62493 | 0.74993 | 0.87491 | 0.99991 | 1.12491 | 1.24991 | 1.37491 | 1.49991 | |
| NOT GO gage for major diameter | Min. | 0. 3 0430 | 0.36600 | 0.42770 | 0.48960 | 0.55130 | 0.61320 | 0.73720 | 0.86100 | 0.98480 | 1.10800 | 1.23300 | 1.35480 | 1.47980 | |
| | Max. | 0. 3 0437 | 0.36607 | 0.42777 | 0.48967 | 0.55137 | 0.61327 | 0.73727 | 0.86109 | 0.98489 | 1.10809 | 1.23309 | 1.35489 | 1.47989 | |

TABLE A10 LIMITING DIMENSIONS OF THREAD WORKING GAGES AND PLAIN DIAMETER GAGES FOR ALTERNATE CLASS 5
FIT TAPPED HOLES, AMERICAN NATIONAL COARSE THREAD SERIES

| | | Size, in. | | | | | | | | | | | | | |
|--|--------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--|
| | | 5/16 | 3/8 | 7/16 | 1/2 | 9/16 | 5/8 | 3/4 | 7/8 | 1 | 1 ¹ /8 | 11/4 | 1 ³ /8 | 11/2 | |
| | | Threads-per inch | | | | | | | | | | | | | |
| Limiting Dimensions | | 18 | 16 | 14 | 13 | 12 | 25 | 10 | 9 | 8 | 7 ' | 7 | 6 | 6 | |
| GO Thread Gages for Tapped Holes | | | | | | | 111 | | | | | | | | |
| Major diameter of working gages | Min. Max. | 0.3125 0.3130 | 0.3750 0.3756 | 0.4375 0.4381 | 0.5000 0.5006 | 0.5625 0.5631 | 0.6250 0.6256 | 0.7500 0.7506 | 0.8750 0.8757 | 1.0000 1.0007 | 1.1250 1.1257 | 1.2500 1.2507 | 1.3750 1.3758 | 1.5000 1.5008 | |
| Pitch diameter of working gages | Min. Max. | 0.2764 0.2765 | 0.3344 0.3345 | 0.3911 0.39125 | 0.4500 0.45015 | 0.5084 0.5086 | 0.5660 0.5662 | 0.6850 0.6852 | 0.8028 0.8030 | 0.9188 0.9190 | 1.0322 1.0324 | 1.1572 1.1574 | 1.2667 1.2669 | 1.3917 1.3919 | |
| | | | | | jie | • | | | | | | | | | |
| NOT GO Thread Gages for Tapped Holes | | | | | O | | 1 | | | | | | | | |
| Major diameter of working gages | Max. Min. | 0.3031 0.3026 | 0.3645 0.3639 | 0.4252 0.4246 | 0.4867 0.4861 | 0.5480 0.5474 | 0.6090 0.6084 | 0.7320 0.7314 | 0.8546 0.8539 | 0.9766 0.9759 | 1.0978 1.0971 | 1.2228 1.2221 | 1.3426 1.3418 | 1.4679 1.4671 | |
| Pitch diameter of thread working gages for production and inspection | Max. Min. | 0.2790 0.2789 | 0.3374 0.3373 | 0.3943 0.39415 | 0.4534 0.45325 | 0.5119 0.5117 | 0.5696 0.5694 | 0.6887 0.6885 | 0.8065 0.8063 | 0.9225 0.9223 | 1.0359 1.0357 | 1.1609 1.1607 | 1.2704 1.2702 | 1.3957 1.3955 | |
| | | | M | | | | | | | | | | | | |
| Plain Diameter Gages for Tapped Holes | | | \mathcal{O} | | | | | | | | | | | | |
| GO gages for minor diameter | Min. Max. | 0.26220 0.26227 | 0.31860 0.31867 | 0.37360 0.37367 | 0.43130 0.43137 | 0.48820 0.48827 | 0.54440 0.54447 | 0.66140 0.66147 | 0.77680 0.77687 | 0.89010 0.89019 | 0.99980 0.99989 | 1.12480 | 1.22860 1.22869 | 1.35360 1.35369 | |
| NOT GO gages for minor diameter | Max. Min | 0.26820 0.26813 | 0.32540 0.32533 | 0.38130 0.38123 | 0.43960 0.43953 | 0.49720 0.49713 | 0.55420 0.55413 | 0.67220 0.67213 | 0.78880 0.78873 | 0.90360 0.90351 | 1.01520 1.01511 | 1.14020 1.14011 | 1.24660 1.24651 | 1.37160 1.37151 | |

TABLE A11 LIMITING DIMENSIONS OF SETTING PLUG AND THREAD WORKING GAGES AND PLAIN DIAMETER GAGES FOR ALTERNATE CLASS 5 FIT THREADED STUDS, AMERICAN NATIONAL FINE THREAD SERIES

| | | | | | | | | Size | e, in. 🔻 🔽 | 2 | | | | | | |
|---|------|------------------|---------|---------|---------|---------|---------|---------|------------|---------|---------|---------|-----------------|---------|---------|--|
| | | 1/4 | 5/16 | 3/8 | 7/16 | 1/2 | 9/16 | 5/8 | 3/4 | 7/8 | 1 | 11/8 | 11/4 | 13/8 | 11/2 | |
| | | Threads per inch | | | | | | | | | | | | | | |
| Limiting Dimensions | | 28 | 24 | 24 | 20 | 20 | 18 | 18 | 16 | 14 | 14 | 12 | 12 | 12 | 12 | |
| GO Thread Gages for Studs | | | | | | | Ç | 77, | | | | | | | | |
| Major diameter of full-form setting plug and full portion of truncated setting plug | Max. | 0.2544 | 0.3172 | 0.3799 | 0.4427 | 0.5055 | 0.5686 | 0.6311 | 0.7565 | 0.8821 | 1.0075 | 1.1331 | 1. 2 578 | 1.3823 | 1.5068 | |
| | Min. | 0.2539 | 0.3167 | 0.3794 | 0.4422 | 0.5050 | 0.5681 | 0.6306 | 0.7559 | 0.8815 | 1.0069 | 1.1325 | 1.2572 | 1.3817 | 1.5062 | |
| Major diameter of truncated portion of | Max. | 0.2438 | 0.3059 | 0.3684 | 0.4303 | 0.4928 | 0.5543 | 0.6168 | 0.7410 | 0.8652 | 0.9902 | 1.1138 | 1.2388 | 1.3638 | 1.4888 | |
| truncated setting plug | Min. | 0.2433 | 0.3054 | 0.3679 | 0.4298 | 0.4923 | 0.5538 | 0.6163 | 0.7404 | 0.8646 | 0.9896 | 1.1132 | 1.2382 | 1.3632 | 1.4882 | |
| Pitch diameter of setting plug and working gage | Max. | 0.2307 | 0.2896 | 0.3523 | 0.4097 | 0.4725 | 0.5320 | 0.5945 | 0.7153 | 0.8351 | 0.9605 | 1.0784 | 1.2031 | 1.3276 | 1.4521 | |
| | Min. | 0.2306 | 0.2895 | 0.3522 | 0.4096 | 0.4724 | 0.53185 | 0.59435 | 0.7151 | 0.8349 | 0.9603 | 1.0782 | 1.2029 | 1.3274 | 1.4519 | |
| Minor diameter of gages | Max. | 0.2152 | 0.2716 | 0.3343 | 0.3881 | 0.4509 | 0.5080 | 0.5705 | 0.6882 | 0.8042 | 0.9296 | 1.0423 | 1.1670 | 1.2915 | 1.4160 | |
| | Min. | 0.2147 | 0.2711 | 0.3338 | 0.3876 | 0.4504 | 0.5075 | 0.5700 | 0.6876 | 0.8036 | 0.9290 | 1.0417 | 1.1664 | 1.2909 | 1.4154 | |
| NOT GO Thread Gages for Studs | : | | | 1 | • | | | | | | | | | | | |
| Major diameter of full-form setting plug and full portion of truncated setting plug | Min. | 0.2539 | 0.3167 | 0.3794 | 0.4422 | 0.5050 | 0.5681 | 0.6306 | 0.7559 | 0.8815 | 1.0069 | 1.1325 | 1.2572 | 1.3817 | 1.5062 | |
| | Max. | 0.2544 | 0.3172 | 0.3799 | 0.4427 | 0.5055 | 0.5686 | 0.6311 | 0.7565 | 0.8821 | 1.0075 | 1.1331 | 1.2578 | 1.3823 | 1.5068 | |
| Major diameter of truncated portion of | Min. | 0.2446 | 0.3059 | 0.3686 | 0.4295 | 0.4923 | 0.5541 | 0.6166 | 0.7402 | 0.8636 | 0.9890 | 1.1119 | 1.2366 | 1.3611 | 1.4856 | |
| truncated setting plug | Max. | 0.2451 | 0.3064 | 0.3691 | 0.4300 | 0.4928 | 0.5546 | 0.6171 | 0.7408 | 0.8642 | 0.9896 | 1.1125 | 1.2372 | 1.3617 | 1.4862 | |
| Pitch diameter of setting plug and working gages for production and inspection | Min. | 0.2296 | 0.2884 | 0.3511 | 0.4084 | 0.4712 | 0.5305 | 0.5930 | 0.7137 | 0.8333 | 0.9587 | 1.0764 | 1.2011 | 1.3256 | 1.4501 | |
| | Max. | 0.2297 | 0.2885 | 0.3512 | 0.4085 | 0.4713 | 0.53065 | 0.59315 | 0.7139 | 0.8335 | 0.9589 | 1.0766 | 1.2013 | 1.3258 | 1.4503 | |
| Plain Diameter Gages for Studs | 1 | O , | | | | | | | | | | | | | | |
| GO gages for major diameter | Max. | 0.25000 | 0.31250 | 0.37500 | 0.43750 | 0.50000 | 0.56250 | 0.62500 | 0.75000 | 0.87500 | 1.00000 | 1.12500 | 1.25000 | 1.37500 | 1.50000 | |
| | Min. | 0.24993 | 0.31243 | 0.37493 | 0.43743 | 0.49993 | 0.56243 | 0.62493 | 0.74993 | 0.87491 | 0.99991 | 1.12491 | 1.24991 | 1.37491 | 1.49991 | |
| NOT GO gages for major diameter | Min. | 0.24380 | 0.30590 | 0.36840 | 0.43030 | 0.49280 | 0.55430 | 0.61680 | 0.74100 | 0.86520 | 0.99020 | 1.11380 | 1.23880 | 1.36380 | 1.48880 | |
| | Max. | 0.24387 | 0.30597 | 0.36847 | 0.43037 | 0.49287 | 0.55437 | 0.61687 | 0.74107 | 0.86529 | 0.99029 | 1.11389 | 1.23889 | 1.36389 | 1.48889 | |

TABLE A12 LIMITING DIMENSIONS OF THREAD WORKING GAGES AND PLAIN DIAMETER GAGES FOR ALTERNATE CLASS 5
FIT TAPPED HOLES, AMERICAN NATIONAL FINE THREAD SERIES

| | | | Size, in. | | | | | | | | | | | | | |
|---|--------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--|
| | | 1/4 | 5/16 | 3/8 | 7/16 | 1/2 | 9/16 | 5/8 | 3/4 | 7/8 | 1 | 11/8 | 11/4 | 13/8 | 11/2 | |
| | | Threads per inch | | | | | | | | | | | | | | |
| Limiting Dimensions | 28 | 24 | 24 | 20 | 20 | 18 | 18 | 16 | 14 | 14 | 12 | 12 | 12 | 12 | | |
| GO Thread Gages for Tapped Holes | | | | | | | | | | | | | | | | |
| Major diameter of working gage | Min. Max. | 0.2500 0.2505 | 0.3125 0.3130 | 0.3750 0.3755 | 0.4375 0.4380 | 0.5000 0.5005 | 0.5625 0.5630 | 0.6250 0.6255 | 0.7500 0.7506 | 0.8750 0.8756 | 1.0000 | 1.1250 1.1256 | 1.2500 1.2506 | 1.3750 1.3756 | 1.5000 1.5006 | |
| Pitch diameter of working gage | Min. Max. | 0.2268 0.2269 | 0.2854 0.2855 | 0.3479 0.3480 | 0.4050 0.4051 | 0.4675 0.4676 | 0.5264 0.52655 | 0.5889 0.58905 | 0.7094 0.7096 | 0.8286 0.8288 | 0.9536 0.9538 | 1.0709 | 1.1959 1.1961 | 1.3209 | 1.4459 | |
| NOT GO Thread Gages for Tapped Holes | | | | | | 07. | | | | | | | | | | |
| Major diameter of working gage | Max. Min. | 0.2445 0.2440 | 0.3058 0.3053 | 0.3683 0.3678 | 0.4293 0.4288 | 0.4918 0.4913 | 0.5535 0.5530 | 0.6160 0.6155 | 0.7397 0.7391 | 0.8631 0.8625 | 0.9881 0.9875 | 1.1110 1.1104 | 1.2357 1.2351 | 1.3602 1.3596 | 1.4847 1.4841 | |
| Pitch diameter of thread working gages for production and inspection | Max. Min. | 0.2290 0.2289 | 0.2878 0.2877 | 0.3503 0.3502 | 0.4076 0.4075 | 0.4701 0.4700 | 0.5294 0.52925 | 0.5919 0.59175 | 0.7126 0.7124 | 0.8322 0.8320 | 0.9572 0.9570 | 1.0749 1.0747 | 1.1996 1.1994 | 1.3241 1.3239 | 1.4486 1.4484 | |
| Plain Diameter Gages for Tapped Holes | | | ļ | CO/2 | | | | | | | | | | | | |
| GO gages for minor diameter | Min. Max. | 0.21670 0.21677 | 0.27430 | 0.33680 0.33687 | 0.39240 0.39247 | 0.45490 0.45497 | 0.51220 0.51227 | 0.57470 0.57477 | 0.69360 0.69367 | 0.81110 0.81117 | 0.93610 0.93619 | 1.05070 1.05079 | 1.17570 1.17579 | 1.30070 1.30079 | 1.42570 1.42579 | |
| NOT GO gages for minor diameter | Max. Min. | 0.22060 0.22053 | 0.27880 0.27873 | 0.34130 0.34123 | 0.39780 0.39773 | 0.46030 0.46023 | 0.51820 0.51813 | 0.58070 0.58063 | 0.70040 0.70033 | 0.81880 0.81873 | 0.94380 0.94371 | 1.05970 1.05961 | 1.18470 1.18461 | 1.30970 1.30961 | 1.43470 1.43461 | |

Intentionally left blank

Ashthorhoc.com.cide.to

APPENDIX B Specifications for Elastic Interference-Fit Thread

(This Appendix is not part of ASME/ANSI B1.12-1987, and is included for information purposes only

B1 INTRODUCTION

Appendix B contains useful information that is supplementary to this Standard.

The elastic interference-fit threads are precision threads. The stud and hole are matched for maximum interference. Studs are hardened steel, CRES (corrosion resistant steel), Monel (Monel 400), B16 (ASTM A 193 High Temperature Alloy Steel B16), and K Monel (Monel K500) set in HY-80 steel (80,000 psi yield strength), HTS (high tensile steel hull plate), and cast Monel (Monel 410). Specifications have also proven satisfactory for nonferrous materials. With good geometry parts, successful interference fits with satisfactory resistance to breakloose torque and minimum distortion to the thread form are common. Percentages of interference metal per turn, compared to maximum interference for NC-5 HF/IF at 100%, are greatly reduced for the elastic flow interference-fit thread (see Appendix D, Table D1). These threads are used in ship construction.

B2 THREAD DESIGNATION

B2.1 Class 5 External Thread Made in Monel and Hard Ferrous Material

EXAMPLE: 0.625-11 NC-5 HFM where

0.625 = nominal size

11 = threads per inch

N = American National thread form

C = coarse thread series

5 = Class 5 Modified tolerance

HF = hard ferrous external thread

M = Monel and K Monel

B2.2 Class 5 Internal Thread Made in Monel, K Monel, and Entire Ferrous Material Hardness Range

EXAMPLE: 0.625-11 NC-5 IFM

where

0.625 = nominal size

11 = threads per inch

N = American National thread form

Ce coarse thread series

5 = Class 5 Modified tolerance

I = internal thread

FM = ferrous, Monel, and K Monel materials

B3 EXTERNAL AND INTERNAL THREADS COMPARED TO NC-5

Examination of Tables B1, B2, and B3 on limits of size, tap drill size, length of engagement, and torque reveals the following.

B3.1 Tolerances

Tolerances are smaller than standard National Class 5 threads for ferrous materials.

B3.2 External Thread

- (a) Maximum major diameter is much smaller than the standard NC-5 threads. The major diameter allowance is approximately equal to 0.020d + 0.001 in.
- (b) Major diameter tolerance is 0.002 in. for $\frac{1}{4}$, $\frac{5}{16}$, and $\frac{3}{8}$ sizes, 0.003 in. for $\frac{7}{16}$ size, and 0.004 in. for $\frac{1}{2}$ in. size and larger.
- (c) Pitch diameter is always larger than basic pitch diameter.
- (d) Pitch diameter tolerance is 0.001 in. for $\frac{3}{8}$ in. and smaller and 0.002 in. for $\frac{9}{6}$ in. and larger.

- (e) Maximum minor diameter is smaller than basic by 0.006 in. to 0.026 in.
 - (f) Minimum minor diameter is specified.

B3.3 Internal Thread

- (a) Minimum minor diameter is from 0.005 in. to 0.041 in. greater than basic.
- (b) Minor diameter tolerance is from 0.008 in. to 0.027 in.
- (c) Minimum pitch diameter is 0.0003 in. to 0.0023 in. larger than basic pitch diameter.
- (d) Pitch diameter tolerances increase from 0.0005 in. to 0.0011 in. between $\frac{1}{4}$ in. and 2 in. sizes.
 - (e) Minimum major diameter is nominal size.
- (f) Taps have a minimum and maximum pitch diameter tolerance specified.

B3.4 Torque

For assemblies made without a locking resin, the minimum assembly torque shall meet the minimum torque values tabulated in Table B3 or shall be at least one and one-half times the breakloose torque.

B4 APPLICATION PRACTICE FOR NEW AND REWORKED EXTERNAL AND INTERNAL THREADS

B4.1 Additional Conditions of Usage (See Section 10)

The following are for elastic interference-fit threads on which satisfactory application of products made to dimensions in Tables B1 and B2 are predicated.

- **B4.1.1 External Thread.** Studs are measured by size-indicating gages and selected to be within 0.0005 in. of the maximum-interference functional size specified in Table B3 for a reworked tapped hole. The stud shall be of uniform quality and condition and shall not have fins, seams, laps, cracks, burrs, an irregular surface, or other injurious defects detrimental to the performance of the part. The geometry of the stud requires that the measured difference between functional size and pitch diameter size does not exceed 50% of the pitch diameter tolerance.
- **B4.1.2 Internal Thread.** Tapped holes are measured by size-indicating gages. Negative taper in hole (small at entering end) is not permitted. Holes shall be bottom tapped. Geometry of profile and hole is controlled by requiring the difference between measured functional size and pitch diameter size to be within 50%

of the pitch diameter tolerance. A hole with a defective thread profile, prior to reassembly, is repaired by retapping with the next larger tap until the profile is restored. Holes are remeasured and studs are matched to holes. In other cases, holes are enlarged to tabulated size to accept stock studs intended for reworking.

B4.1.3 Pitch Diameter Interference

- (a) Maximum Pitch Diameter Interference. Selection of thread assemblies for maximum pitch diameter interference will ensure that the torque values tabulated in Table B3 will be met.
- (b) Minimum Pitch Diameter Interference. An examination of the minimum interference column in Table B3 reveals zero interference on pitch diameter. In practice, when measured external and internal threads are both at minimum material, variations within acceptable limits for lead, angle, taper, roundness, etc., do provide some functional metal-to-metal interference. If the assembly does not meet the torque requirements stated in para. B3.4, a resin sealant may be required to lock the assembly for those applications when sealants are acceptable.
- ➢ B4.1.4 Resin Sealants. Under specified conditions, reworked assemblies with poor interference or clearance may be locked together with anaerobic sealant. These assemblies may not be subject to temperatures above 200°F.

Before applying sealant, clean parts with oil-free cleaner, dry, and prime with MIL-S-22773 Grade N. Let dry. Use sealant MIL-S-22773 Grade AV when clearance is under 0.005 in. and Grade AVV for larger clearances.

- **B4.1.5 Surface Roughness.** The optimum surface roughness for both external and internal threads was found to be 63 μ in. Ra. Values under 125 μ in. Ra are recommended. Rougher surfaces are fractured and may release bits of metal during the engagement and get trapped in the interference zone. This results in the need for greater torque with heat generation which may produce more assembly failures. Surface roughness less than 63 μ in. Ra may inhibit flow of lubricant, permit buildup of hydraulic pressure, and require higher assembly torque.
- **B4.1.6 Driving Speed.** Torque should be applied smoothly and evenly. Torque readings should continually increase as the length of engagement becomes greater. When K Monel studs are driven into Monel or K Monel holes, a great deal of heat is generated. Driving should be stopped several times to let the heat dissipate. When excessive torque builds up, backing off one or two turns before driving the stud home may re-

duce the torque 30 or 40 lb-ft on a 5% in. thread. The mechanic must determine the optimum driving speed, because type of lubricant, hardness, surface texture, and materials vary with the application.

B4.1.7 Assembly and Disassembly. A set stud must resist rotation when seating and breaking away the prevailing torque nut. Otherwise, the assembly is a failure. After studs are seated, the end faces are scribed with lines, all directed toward the center of the component or some designated point. Rotation resulting from movement of prevailing torque nut can be easily recognized when lines do not line up. When studs are removed during overhaul, questionable profiles are measured and reworked, if necessary. Reapplication up to four times without reworking is feasible, but assembly torque may decrease 60%.

B4.1.8 Acceptability. Acceptability of elastic interference-fit threads shall be determined based upon System 23 of ANSI/ASME B1.3M. The following modifications of System 23 apply.

Unified Clas in ANSI/ASME in Table B4 if the content of the cont

- (a) Size-indicating gages are required.
- (b) Roundness, lead variation, flank angle variation runout, and surface texture are not required.

NOTE: Application may require one or more of these measurements.

B5 GAGING

B5.1 Limits of Size

The limits of size for maximum-material setting gages, specifically for plug gages for external threads and solid ring gages for internal threads, are tabulated in Table B4. Indicating gages need only one reference gage for setting.

B5.2 Unified Class 3A and 3B Setting Gages

Unified Class 3A and 3B setting gages, as tabulated in ANSI/ASME B1.2, may be substituted for the gages in Table B4 if the indicating gages have sufficient travel.